

LAMPIRAN I
STANDAR PENELITIAN

Berikut adalah perbandingan detail antara **ASTM D638** (sifat tarik plastik) dan **ASTM D1076** (spesifikasi lateks karet alami) dalam bentuk tabel:

Aspek	ASTM D638 (Sifat Tarik Plastik)	ASTM D1076 (Spesifikasi Lateks Karet Alami)
Tujuan	Mengukur sifat tarik plastik seperti kekuatan tarik, modulus elastisitas, elongasi, dll.	Menentukan spesifikasi untuk lateks karet alam terkonsentrasi.
Jenis Material	Plastik (tidak diperkuat dan diperkuat), termasuk lembaran, pelat, dan material cetakan.	Lateks karet alami Hevea atau Guayule dalam 5 kategori.
Ketebalan Material	≤14 mm (0.55 in); material lebih tebal perlu dimachining.	Tidak berlaku batas ketebalan tertentu, fokus pada larutan lateks cair.
Kategori Material	Tidak ada kategori khusus; berlaku untuk semua jenis plastik sesuai spesifikasi uji.	5 kategori lateks berdasarkan metode stabilisasi dan komposisi kimia.
Prosedur Sampling	Spesimen dipotong atau dibentuk sesuai tipe standar (I-V) dan dikondisikan sebelum uji.	Sampel diambil dari drum atau tangki menggunakan metode pencampuran homogen.
Parameter Utama	Kekuatan tarik, elongasi, modulus elastisitas, tegangan pada yield/patah, dll.	Total solids, dry rubber content, protein content, alkalinitas, dll.
Alat Uji	Mesin tarik dengan extensometer, mikrometer untuk dimensi spesimen.	Alat ukur viskositas, pH meter, oven pengering, dan alat titrasi.
Metode Uji	Tarik spesimen hingga patah pada kecepatan tertentu.	Analisis total solids dengan pengeringan.- Titrasi alkalinitas.- Koagulasi lateks untuk pengukuran DRC.
Kondisi Pengujian	Suhu dan kelembapan dikondisikan (ASTM D618).	Suhu dan kelembapan dikondisikan; lateks dicampur hingga homogen sebelum uji.

Aspek	ASTM D638 (Sifat Tarik Plastik)	ASTM D1076 (Spesifikasi Lateks Karet Alami)
Kecepatan Pengujian	5-500 mm/min tergantung spesimen (Tabel dalam D638).	Tidak relevan; parameter fokus pada analisis kimia dan fisik lateks.
Parameter Kimia	Tidak ada pengukuran langsung parameter kimia.	Mengukur protein total, alkalinitas, kandungan logam (Cu, Mn), dan komposisi.
Pelaporan	Identifikasi material, hasil kekuatan tarik, elongasi, modulus elastisitas, dll.	Identifikasi lateks, kandungan kimia, stabilitas mekanis, total solids, dll.
Aplikasi	Digunakan untuk spesifikasi desain plastik dalam aplikasi rekayasa.	Digunakan untuk kontrol kualitas lateks dalam aplikasi industri karet.

Kesimpulan

1. **Ruang Lingkup:** ASTM D638 fokus pada sifat mekanik plastik padat, sementara ASTM D1076 fokus pada spesifikasi kimia dan fisik lateks cair.
2. **Pendekatan Pengujian:** ASTM D638 lebih bersifat mekanis (tarik spesimen hingga patah), sedangkan ASTM D1076 lebih kimiawi dan fisik untuk larutan lateks.
3. **Parameter yang Diukur:** ASTM D638 mengukur kekuatan tarik dan sifat elastisitas, sementara ASTM D1076 lebih banyak mengukur komposisi kimia seperti kandungan protein, alkalinitas, dan stabilitas.



Designation: D638 – 14

Standard Test Method for Tensile Properties of Plastics¹

This standard is issued under the fixed designation D638; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the U.S. Department of Defense.

1. Scope*

1.1 This test method covers the determination of the tensile properties of unreinforced and reinforced plastics in the form of standard dumbbell-shaped test specimens when tested under defined conditions of pretreatment, temperature, humidity, and testing machine speed.

1.2 This test method is applicable for testing materials of any thickness up to 14 mm (0.55 in.). However, for testing specimens in the form of thin sheeting, including film less than 1.0 mm (0.04 in.) in thickness, ASTM standard **D882** is the preferred test method. Materials with a thickness greater than 14 mm (0.55 in.) shall be reduced by machining.

1.3 This test method includes the option of determining Poisson's ratio at room temperature.

NOTE 1—This standard and ISO 527-1 address the same subject matter, but differ in technical content.

NOTE 2—This test method is not intended to cover precise physical procedures. It is recognized that the constant rate of crosshead movement type of test leaves much to be desired from a theoretical standpoint, that wide differences may exist between rate of crosshead movement and rate of strain between gage marks on the specimen, and that the testing speeds specified disguise important effects characteristic of materials in the plastic state. Further, it is realized that variations in the thicknesses of test specimens, which are permitted by these procedures, produce variations in the surface-volume ratios of such specimens, and that these variations may influence the test results. Hence, where directly comparable results are desired, all samples should be of equal thickness. Special additional tests should be used where more precise physical data are needed.

NOTE 3—This test method may be used for testing phenolic molded resin or laminated materials. However, where these materials are used as electrical insulation, such materials should be tested in accordance with Test Methods **D229** and Test Method **D651**.

NOTE 4—For tensile properties of resin-matrix composites reinforced with oriented continuous or discontinuous high modulus >20 -GPa ($>3.0 \times 10^6$ -psi) fibers, tests shall be made in accordance with Test Method **D3039/D3039M**.

1.4 Test data obtained by this test method have been found to be useful in engineering design. However, it is important to

consider the precautions and limitations of this method found in **Note 2** and **Section 4** before considering these data for engineering design.

1.5 The values stated in SI units are to be regarded as standard. The values given in parentheses are for information only.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

- D229** Test Methods for Rigid Sheet and Plate Materials Used for Electrical Insulation
- D412** Test Methods for Vulcanized Rubber and Thermoplastic Elastomers—Tension
- D618** Practice for Conditioning Plastics for Testing
- D651** Test Method for Test for Tensile Strength of Molded Electrical Insulating Materials (Withdrawn 1989)³
- D882** Test Method for Tensile Properties of Thin Plastic Sheet
- D883** Terminology Relating to Plastics
- D1822** Test Method for Tensile-Impact Energy to Break Plastics and Electrical Insulating Materials
- D3039/D3039M** Test Method for Tensile Properties of Polymer Matrix Composite Materials
- D4000** Classification System for Specifying Plastic Materials
- D4066** Classification System for Nylon Injection and Extrusion Materials (PA)
- D5947** Test Methods for Physical Dimensions of Solid Plastics Specimens
- E4** Practices for Force Verification of Testing Machines

¹ This test method is under the jurisdiction of ASTM Committee **D20** on Plastics and is the direct responsibility of Subcommittee **D20.10** on Mechanical Properties.

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ The last approved version of this historical standard is referenced on www.astm.org.

*A Summary of Changes section appears at the end of this standard

E83 Practice for Verification and Classification of Extensometer Systems

E132 Test Method for Poisson's Ratio at Room Temperature

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

2.2 *ISO Standard*.⁴

ISO 527-1 Determination of Tensile Properties

3. Terminology

3.1 *Definitions*—Definitions of terms applying to this test method appear in Terminology **D883** and **Annex A2**.

4. Significance and Use

4.1 This test method is designed to produce tensile property data for the control and specification of plastic materials. These data are also useful for qualitative characterization and for research and development.

4.2 Some material specifications that require the use of this test method, but with some procedural modifications that take precedence when adhering to the specification. Therefore, it is advisable to refer to that material specification before using this test method. Table 1 in Classification **D4000** lists the ASTM materials standards that currently exist.

4.3 Tensile properties are known to vary with specimen preparation and with speed and environment of testing. Consequently, where precise comparative results are desired, these factors must be carefully controlled.

4.4 It is realized that a material cannot be tested without also testing the method of preparation of that material. Hence, when comparative tests of materials per se are desired, exercise great care to ensure that all samples are prepared in exactly the same way, unless the test is to include the effects of sample preparation. Similarly, for referee purposes or comparisons within any given series of specimens, care shall be taken to secure the maximum degree of uniformity in details of preparation, treatment, and handling.

4.5 Tensile properties provide useful data for plastics engineering design purposes. However, because of the high degree of sensitivity exhibited by many plastics to rate of straining and environmental conditions, data obtained by this test method cannot be considered valid for applications involving load-time scales or environments widely different from those of this test method. In cases of such dissimilarity, no reliable estimation of the limit of usefulness can be made for most plastics. This sensitivity to rate of straining and environment necessitates testing over a broad load-time scale (including impact and creep) and range of environmental conditions if tensile properties are to suffice for engineering design purposes.

NOTE 5—Since the existence of a true elastic limit in plastics (as in many other organic materials and in many metals) is debatable, the propriety of applying the term “elastic modulus” in its quoted, generally accepted definition to describe the “stiffness” or “rigidity” of a plastic has been seriously questioned. The exact stress-strain characteristics of plastic materials are highly dependent on such factors as rate of application of

stress, temperature, previous history of specimen, etc. However, stress-strain curves for plastics, determined as described in this test method, almost always show a linear region at low stresses, and a straight line drawn tangent to this portion of the curve permits calculation of an elastic modulus of the usually defined type. Such a constant is useful if its arbitrary nature and dependence on time, temperature, and similar factors are realized.

5. Apparatus

5.1 *Testing Machine*—A testing machine of the constant-rate-of-crosshead-movement type and comprising essentially the following:

5.1.1 *Fixed Member*—A fixed or essentially stationary member carrying one grip.

5.1.2 *Movable Member*—A movable member carrying a second grip.

5.1.3 *Grips*—Grips for holding the test specimen between the fixed member and the movable member of the testing machine can be either the fixed or self-aligning type.

5.1.3.1 Fixed grips are rigidly attached to the fixed and movable members of the testing machine. When this type of grip is used take extreme care to ensure that the test specimen is inserted and clamped so that the long axis of the test specimen coincides with the direction of pull through the center line of the grip assembly.

5.1.3.2 Self-aligning grips are attached to the fixed and movable members of the testing machine in such a manner that they will move freely into alignment as soon as any load is applied so that the long axis of the test specimen will coincide with the direction of the applied pull through the center line of the grip assembly. Align the specimens as perfectly as possible with the direction of pull so that no rotary motion that may induce slippage will occur in the grips; there is a limit to the amount of misalignment self-aligning grips will accommodate.

5.1.3.3 The test specimen shall be held in such a way that slippage relative to the grips is prevented insofar as possible. Grip surfaces that are deeply scored or serrated with a pattern similar to those of a coarse single-cut file, serrations about 2.4 mm (0.09 in.) apart and about 1.6 mm (0.06 in.) deep, have been found satisfactory for most thermoplastics. Finer serrations have been found to be more satisfactory for harder plastics, such as the thermosetting materials. It is important that the serrations be kept clean and sharp. Should breaking in the grips occur, even when deep serrations or abraded specimen surfaces are used, other techniques shall be used. Other techniques that have been found useful, particularly with smooth-faced grips, are abrading that portion of the surface of the specimen that will be in the grips, and interposing thin pieces of abrasive cloth, abrasive paper, or plastic, or rubber-coated fabric, commonly called hospital sheeting, between the specimen and the grip surface. No. 80 double-sided abrasive paper has been found effective in many cases. An open-mesh fabric, in which the threads are coated with abrasive, has also been effective. Reducing the cross-sectional area of the specimen may also be effective. The use of special types of grips is sometimes necessary to eliminate slippage and breakage in the grips.

5.1.4 *Drive Mechanism*—A drive mechanism for imparting a uniform, controlled velocity to the movable member with

⁴ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

respect to the stationary member. This velocity is to be regulated as specified in Section 8.

5.1.5 Load Indicator—A suitable load-indicating mechanism capable of showing the total tensile load carried by the test specimen when held by the grips. This mechanism shall be essentially free of inertia lag at the specified rate of testing and shall indicate the load with an accuracy of $\pm 1\%$ of the indicated value, or better. The accuracy of the testing machine shall be verified in accordance with Practices E4.

NOTE 6—Experience has shown that many testing machines now in use are incapable of maintaining accuracy for as long as the periods between inspection recommended in Practices E4. Hence, it is recommended that each machine be studied individually and verified as often as may be found necessary. It frequently will be necessary to perform this function daily.

5.1.6 The fixed member, movable member, drive mechanism, and grips shall be constructed of such materials and in such proportions that the total elastic longitudinal strain of the system constituted by these parts does not exceed 1 % of the total longitudinal strain between the two gage marks on the test specimen at any time during the test and at any load up to the rated capacity of the machine.

5.1.7 Crosshead Extension Indicator—A suitable extension indicating mechanism capable of showing the amount of change in the separation of the grips, that is, crosshead movement. This mechanism shall be essentially free of inertial lag at the specified rate of testing and shall indicate the crosshead movement with an accuracy of $\pm 10\%$ of the indicated value.

5.2 Extension Indicator (extensometer)—A suitable instrument shall be used for determining the distance between two designated points within the gauge length of the test specimen as the specimen is stretched. For referee purposes, the extensometer must be set at the full gage length of the specimen, as shown in Fig. 1. It is desirable, but not essential, that this instrument automatically record this distance, or any change in it, as a function of the load on the test specimen or of the elapsed time from the start of the test, or both. If only the latter is obtained, load-time data must also be taken. This instrument shall be essentially free of inertia at the specified speed of testing. Extensometers shall be classified and their calibration periodically verified in accordance with Practice E83.

5.2.1 Modulus-of-Elasticity Measurements—For modulus-of-elasticity measurements, an extensometer with a maximum strain error of 0.0002 mm/mm (in./in.) that automatically and continuously records shall be used. An extensometer classified by Practice E83 as fulfilling the requirements of a B-2 classification within the range of use for modulus measurements meets this requirement.

5.2.2 Low-Extension Measurements—For elongation-at-yield and low-extension measurements (nominally 20 % or less), the same above extensometer, attenuated to 20 % extension, is acceptable. In any case, the extensometer system must meet at least Class C (Practice E83) requirements, which include a fixed strain error of 0.001 strain or $\pm 1.0\%$ of the indicated strain, whichever is greater.

5.2.3 High-Extension Measurements—For making measurements at elongations greater than 20 %, measuring techniques with error no greater than $\pm 10\%$ of the measured value are acceptable.

5.3 Micrometers—Apparatus for measuring the width and thickness of the test specimen shall comply with the requirements of Test Method D5947.

6. Test Specimens

6.1 Sheet, Plate, and Molded Plastics:

6.1.1 Rigid and Semirigid Plastics—The test specimen shall conform to the dimensions shown in Fig. 1. The Type I specimen is the preferred specimen and shall be used where sufficient material having a thickness of 7 mm (0.28 in.) or less is available. The Type II specimen is recommended when a material does not break in the narrow section with the preferred Type I specimen. The Type V specimen shall be used where only limited material having a thickness of 4 mm (0.16 in.) or less is available for evaluation, or where a large number of specimens are to be exposed in a limited space (thermal and environmental stability tests, etc.). The Type IV specimen is generally used when direct comparisons are required between materials in different rigidity cases (that is, nonrigid and semirigid). The Type III specimen must be used for all materials with a thickness of greater than 7 mm (0.28 in.) but not more than 14 mm (0.55 in.).

6.1.2 Nonrigid Plastics—The test specimen shall conform to the dimensions shown in Fig. 1. The Type IV specimen shall be used for testing nonrigid plastics with a thickness of 4 mm (0.16 in.) or less. The Type III specimen must be used for all materials with a thickness greater than 7 mm (0.28 in.) but not more than 14 mm (0.55 in.).

6.1.3 Reinforced Composites—The test specimen for reinforced composites, including highly orthotropic laminates, shall conform to the dimensions of the Type I specimen shown in Fig. 1.

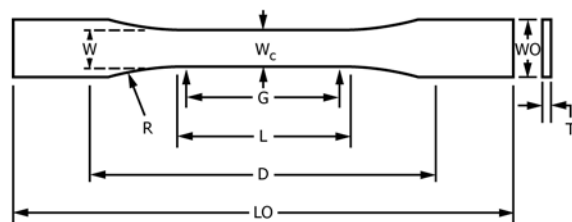
6.1.4 Preparation—Methods of preparing test specimens include injection molding, machining operations, or die cutting, from materials in sheet, plate, slab, or similar form. Materials thicker than 14 mm (0.55 in.) shall be machined to 14 mm (0.55 in.) for use as Type III specimens.

NOTE 7—Test results have shown that for some materials such as glass cloth, SMC, and BMC laminates, other specimen types should be considered to ensure breakage within the gage length of the specimen, as mandated by 7.3.

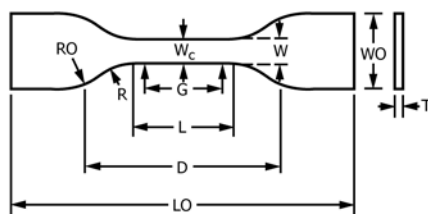
NOTE 8—When preparing specimens from certain composite laminates such as woven roving, or glass cloth, exercise care in cutting the specimens parallel to the reinforcement. The reinforcement will be significantly weakened by cutting on a bias, resulting in lower laminate properties, unless testing of specimens in a direction other than parallel with the reinforcement constitutes a variable being studied.

NOTE 9—Specimens prepared by injection molding may have different tensile properties than specimens prepared by machining or die-cutting because of the orientation induced. This effect may be more pronounced in specimens with narrow sections.

6.2 Rigid Tubes—The test specimen for rigid tubes shall be as shown in Fig. 2. The length, L , shall be as shown in the table in Fig. 2. A groove shall be machined around the outside of the specimen at the center of its length so that the wall section after



TYPES I, II, III & V



TYPE IV

Specimen Dimensions for Thickness, T , mm (in.)^A

Dimensions (see drawings)	7 (0.28) or under		Over 7 to 14 (0.28 to 0.55), incl	4 (0.16) or under		Tolerances
	Type I	Type II	Type III	Type IV ^B	Type V ^{C,D}	
W—Width of narrow section ^{E,F}	13 (0.50)	6 (0.25)	19 (0.75)	6 (0.25)	3.18 (0.125)	±0.5 (±0.02) ^{B,C}
L—Length of narrow section	57 (2.25)	57 (2.25)	57 (2.25)	33 (1.30)	9.53 (0.375)	±0.5 (±0.02) ^C
WO—Width overall, min ^G	19 (0.75)	19 (0.75)	29 (1.13)	19 (0.75)	...	+ 6.4 (+ 0.25)
WO—Width overall, min ^G	9.53 (0.375)	+ 3.18 (+ 0.125)
LO—Length overall, min ^H	165 (6.5)	183 (7.2)	246 (9.7)	115 (4.5)	63.5 (2.5)	no max (no max)
G—Gage length ^I	50 (2.00)	50 (2.00)	50 (2.00)	...	7.62 (0.300)	±0.25 (±0.010) ^C
G—Gage length ^I	25 (1.00)	...	±0.13 (±0.005)
D—Distance between grips	115 (4.5)	135 (5.3)	115 (4.5)	65 (2.5) ^J	25.4 (1.0)	±5 (±0.2)
R—Radius of fillet	76 (3.00)	76 (3.00)	76 (3.00)	14 (0.56)	12.7 (0.5)	±1 (±0.04) ^C
RO—Outer radius (Type IV)	25 (1.00)	...	±1 (±0.04)

^AThickness, T , shall be 3.2 ± 0.4 mm (0.13 ± 0.02 in.) for all types of molded specimens, and for other Types I and II specimens where possible. If specimens are machined from sheets or plates, thickness, T , shall be the thickness of the sheet or plate provided this does not exceed the range stated for the intended specimen type. For sheets of nominal thickness greater than 14 mm (0.55 in.) the specimens shall be machined to 14 ± 0.4 mm (0.55 ± 0.02 in.) in thickness, for use with the Type III specimen. For sheets of nominal thickness between 14 and 51 mm (0.55 and 2 in.) approximately equal amounts shall be machined from each surface. For thicker sheets both surfaces of the specimen shall be machined, and the location of the specimen with reference to the original thickness of the sheet shall be noted. Tolerances on thickness less than 14 mm (0.55 in.) shall be those standard for the grade of material tested.

^BFor the Type IV specimen, the internal width of the narrow section of the die shall be 6.00 ± 0.05 mm (0.250 ± 0.002 in.). The dimensions are essentially those of Die C in Test Methods D412.

^CThe Type V specimen shall be machined or die cut to the dimensions shown, or molded in a mold whose cavity has these dimensions. The dimensions shall be:

$W = 3.18 \pm 0.03$ mm (0.125 ± 0.001 in.),

$L = 9.53 \pm 0.08$ mm (0.375 ± 0.003 in.),

$G = 7.62 \pm 0.02$ mm (0.300 ± 0.001 in.), and

$R = 12.7 \pm 0.08$ mm (0.500 ± 0.003 in.).

The other tolerances are those in the table.

^DSupporting data on the introduction of the L specimen of Test Method D1822 as the Type V specimen are available from ASTM Headquarters. Request RR:D20-1038.

^EThe tolerances of the width at the center W_c shall be $+0.00$ mm, -0.10 mm ($+0.000$ in., -0.004 in.) compared with width W at other parts of the reduced section. Any reduction in W at the center shall be gradual, equally on each side so that no abrupt changes in dimension result.

^FFor molded specimens, a draft of not over 0.13 mm (0.005 in.) is allowed for either Type I or II specimens 3.2 mm (0.13 in.) in thickness. See diagram below and this shall be taken into account when calculating width of the specimen. Thus a typical section of a molded Type I specimen, having the maximum allowable draft, could be as follows:

^GOverall widths greater than the minimum indicated are used for some materials in order to avoid breaking in the grips.

^HOverall lengths greater than the minimum indicated are used for some materials to avoid breaking in the grips or to satisfy special test requirements.

^ITest marks or initial extensometer span.

^JWhen self-tightening grips are used, for highly extensible polymers, the distance between grips will depend upon the types of grips used and may not be critical if maintained uniform once chosen.

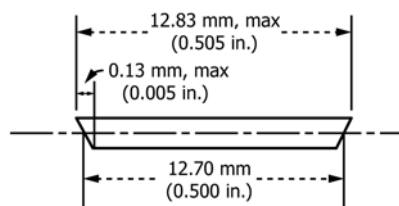
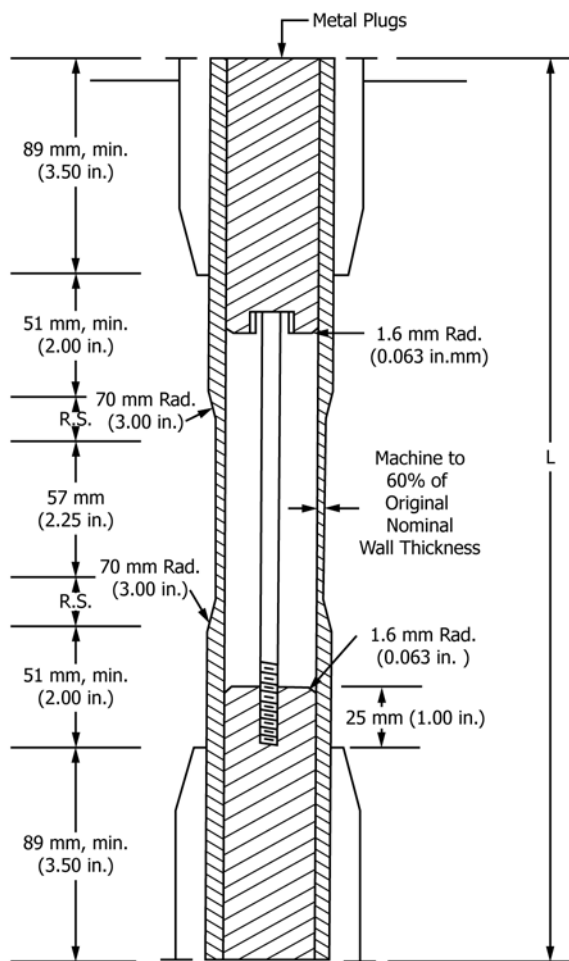


FIG. 1 Tension Test Specimens for Sheet, Plate, and Molded Plastics



DIMENSIONS OF TUBE SPECIMENS

Nominal Wall Thickness	Length of Radial Sections, 2R.S.	Total Calculated Minimum Length of Specimen	Standard Length, L, of Specimen to Be Used for 89-mm (3.5-in.) Jaws ^A
mm (in.)			
0.79 (1/32)	13.9 (0.547)	350 (13.80)	381 (15)
1.2 (3/64)	17.0 (0.670)	354 (13.92)	381 (15)
1.6 (1/16)	19.6 (0.773)	356 (14.02)	381 (15)
2.4 (3/32)	24.0 (0.946)	361 (14.20)	381 (15)
3.2 (1/8)	27.7 (1.091)	364 (14.34)	381 (15)
4.8 (3/16)	33.9 (1.333)	370 (14.58)	381 (15)
6.4 (1/4)	39.0 (1.536)	376 (14.79)	400 (15.75)
7.9 (5/16)	43.5 (1.714)	380 (14.96)	400 (15.75)
9.5 (3/8)	47.6 (1.873)	384 (15.12)	400 (15.75)
11.1 (7/16)	51.3 (2.019)	388 (15.27)	400 (15.75)
12.7 (1/2)	54.7 (2.154)	391 (15.40)	419 (16.5)

^AFor jaws greater than 89 mm (3.5 in.), the standard length shall be increased by twice the length of the jaws minus 178 mm (7 in.). The standard length permits a slippage of approximately 6.4 to 12.7 mm (0.25 to 0.50 in.) in each jaw while maintaining the maximum length of the jaw grip.

FIG. 2 Diagram Showing Location of Tube Tension Test Specimens in Testing Machine

machining shall be 60 % of the original nominal wall thick-

ness. This groove shall consist of a straight section 57.2 mm (2.25 in.) in length with a radius of 76 mm (3 in.) at each end joining it to the outside diameter. Steel or brass plugs having diameters such that they will fit snugly inside the tube and having a length equal to the full jaw length plus 25 mm (1 in.) shall be placed in the ends of the specimens to prevent crushing. They can be located conveniently in the tube by separating and supporting them on a threaded metal rod. Details of plugs and test assembly are shown in Fig. 2.

6.3 *Rigid Rods*—The test specimen for rigid rods shall be as shown in Fig. 3. The length, *L*, shall be as shown in the table in Fig. 3. A groove shall be machined around the specimen at the center of its length so that the diameter of the machined portion shall be 60 % of the original nominal diameter. This groove shall consist of a straight section 57.2 mm (2.25 in.) in length with a radius of 76 mm (3 in.) at each end joining it to the outside diameter.

6.4 All surfaces of the specimen shall be free of visible flaws, scratches, or imperfections. Marks left by coarse machining operations shall be carefully removed with a fine file or abrasive, and the filed surfaces shall then be smoothed with abrasive paper (No. 00 or finer). The finishing sanding strokes shall be made in a direction parallel to the long axis of the test specimen. All flash shall be removed from a molded specimen, taking great care not to disturb the molded surfaces. In machining a specimen, undercuts that would exceed the dimensional tolerances shown in Fig. 1 shall be scrupulously avoided. Care shall also be taken to avoid other common machining errors.

6.5 If it is necessary to place gage marks on the specimen, this shall be done with a wax crayon or India ink that will not affect the material being tested. Gage marks shall not be scratched, punched, or impressed on the specimen.

6.6 When testing materials that are suspected of anisotropy, duplicate sets of test specimens shall be prepared, having their long axes respectively parallel with, and normal to, the suspected direction of anisotropy.

7. Number of Test Specimens

7.1 Test at least five specimens for each sample in the case of isotropic materials.

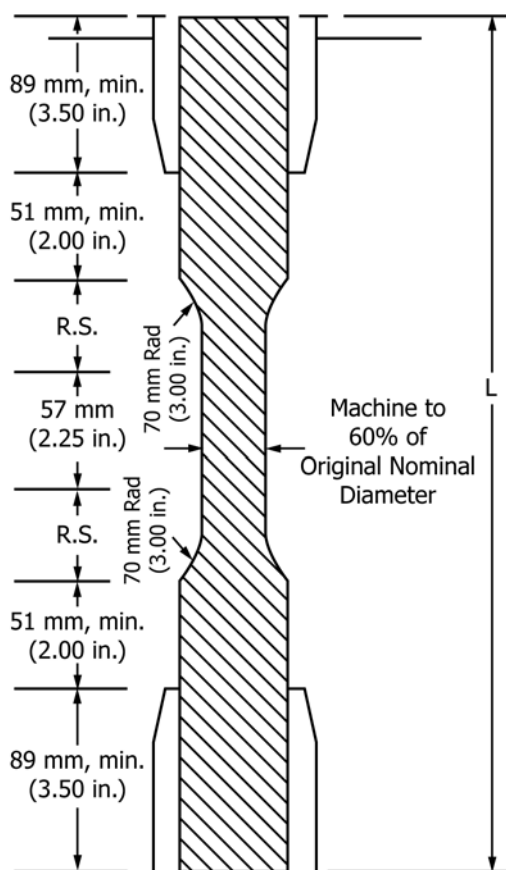
7.2 For anisotropic materials, when applicable, test five specimens, normal to, and five parallel with, the principle axis of anisotropy.

7.3 Discard specimens that break at some flaw, or that break outside of the narrow cross-sectional test section (Fig. 1, dimension “L”), and make retests, unless such flaws constitute a variable to be studied.

NOTE 10—Before testing, all transparent specimens should be inspected in a polariscope. Those which show atypical or concentrated strain patterns should be rejected, unless the effects of these residual strains constitute a variable to be studied.

8. Speed of Testing

8.1 Speed of testing shall be the relative rate of motion of the grips or test fixtures during the test. The rate of motion of the driven grip or fixture when the testing machine is running



DIMENSIONS OF ROD SPECIMENS

Nominal Diameter	Length of Radial Sections, 2R.S.	Total Calculated Minimum Length of Specimen	Standard Length, <i>L</i> , of Specimen to Be Used for 89-mm (3.5-in.) Jaws ^A
mm (in.)			
3.2 (1/8)	19.6 (0.773)	356 (14.02)	381 (15)
4.7 (1/16)	24.0 (0.946)	361 (14.20)	381 (15)
6.4 (1/4)	27.7 (1.091)	364 (14.34)	381 (15)
9.5 (3/8)	33.9 (1.333)	370 (14.58)	381 (15)
12.7 (1/2)	39.0 (1.536)	376 (14.79)	400 (15.75)
15.9 (5/8)	43.5 (1.714)	380 (14.96)	400 (15.75)
19.0 (3/4)	47.6 (1.873)	384 (15.12)	400 (15.75)
22.2 (7/8)	51.5 (2.019)	388 (15.27)	400 (15.75)
25.4 (1)	54.7 (2.154)	391 (15.40)	419 (16.5)
31.8 (1 1/4)	60.9 (2.398)	398 (15.65)	419 (16.5)
38.1 (1 1/2)	66.4 (2.615)	403 (15.87)	419 (16.5)
42.5 (1 3/4)	71.4 (2.812)	408 (16.06)	419 (16.5)
50.8 (2)	76.0 (2.993)	412 (16.24)	432 (17)

^AFor jaws greater than 89 mm (3.5 in.), the standard length shall be increased by twice the length of the jaws minus 178 mm (7 in.). The standard length permits a slippage of approximately 6.4 to 12.7 mm (0.25 to 0.50 in.) in each jaw while maintaining the maximum length of the jaw grip.

FIG. 3 Diagram Showing Location of Rod Tension Test Specimen in Testing Machine

idle may be used, if it can be shown that the resulting speed of testing is within the limits of variation allowed.

8.2 Choose the speed of testing from Table 1. Determine this chosen speed of testing by the specification for the material being tested, or by agreement between those concerned. When

TABLE 1 Designations for Speed of Testing^A

Classification ^B	Specimen Type	Speed of Testing, mm/min (in./min)	Nominal Strain ^C Rate at Start of Test, mm/mm·min (in./in·min)
Rigid and Semirigid	I, II, III rods and tubes	5 (0.2) ± 25 %	0.1
		50 (2) ± 10 %	1
		500 (20) ± 10 %	10
	IV	5 (0.2) ± 25 %	0.15
		50 (2) ± 10 %	1.5
	V	500 (20) ± 10 %	15
Nonrigid	III	1 (0.05) ± 25 %	0.1
		10 (0.5) ± 25 %	1
		100 (5) ± 25 %	10
	IV	50 (2) ± 10 %	1
		500 (20) ± 10 %	10
		50 (2) ± 10 %	1.5

^ASelect the lowest speed that produces rupture in 0.5 to 5 min for the specimen geometry being used (see 8.2).

^BSee Terminology D883 for definitions.

^CThe initial rate of straining cannot be calculated exactly for dumbbell-shaped specimens because of extension, both in the reduced section outside the gage length and in the fillets. This initial strain rate can be measured from the initial slope of the tensile strain-versus-time diagram.

the speed is not specified, use the lowest speed shown in Table 1 for the specimen geometry being used, which gives rupture within 0.5 to 5-min testing time.

8.3 Make modulus determinations at the speed selected for the other tensile properties when the recorder response and resolution are adequate.

9. Conditioning

9.1 *Conditioning*—Condition the test specimens in accordance with Procedure A of Practice D618, unless otherwise specified by contract or the relevant ASTM material specification. Conditioning time is specified as a minimum. Temperature and humidity tolerances shall be in accordance with Section 7 of Practice D618 unless specified differently by contract or material specification.

9.2 *Test Conditions*—Conduct the tests at the same temperature and humidity used for conditioning with tolerances in accordance with Section 7 of Practice D618, unless otherwise specified by contract or the relevant ASTM material specification.

10. Procedure

10.1 Measure the width and thickness of each specimen to the nearest 0.025 mm (0.001 in.) using the applicable test methods in D5947.

10.1.1 Measure the width and thickness of flat specimens at the center of each specimen and within 5 mm of each end of the gage length.

10.1.2 For injection molded specimens, the actual measurement of only one specimen from each sample will suffice when it has previously been demonstrated that the specimen-to-specimen variation in width and thickness is less than 1 %.

10.1.3 For thin sheeting, including film less than 1.0 mm (0.04 in.), take the width of specimens produced by a Type IV die as the distance between the cutting edges of the die in the

narrow section. For all other specimens, measure the actual width of the center portion of the specimen to be tested, unless it can be shown that the actual width of the specimen is the same as that of the die within the specimen dimension tolerances given in Fig. 1.

10.1.4 Measure the diameter of rod specimens, and the inside and outside diameters of tube specimens, to the nearest 0.025 mm (0.001 in.) at a minimum of two points 90° apart; make these measurements along the groove for specimens so constructed. Use plugs in testing tube specimens, as shown in Fig. 2.

10.2 Place the specimen in the grips of the testing machine, taking care to align the long axis of the specimen and the grips with an imaginary line joining the points of attachment of the grips to the machine. The distance between the ends of the gripping surfaces, when using flat specimens, shall be as indicated in Fig. 1. On tube and rod specimens, the location for the grips shall be as shown in Fig. 2 and Fig. 3. Tighten the grips evenly and firmly to the degree necessary to prevent slippage of the specimen during the test, but not to the point where the specimen would be crushed.

10.3 Attach the extension indicator. When modulus is being determined, a Class B-2 or better extensometer is required (see 5.2.1).

NOTE 11—Modulus of materials is determined from the slope of the linear portion of the stress-strain curve. For most plastics, this linear portion is very small, occurs very rapidly, and must be recorded automatically. The change in jaw separation is never to be used for calculating modulus or elongation.

10.4 Set the speed of testing at the proper rate as required in Section 8, and start the machine.

10.5 Record the load-extension curve of the specimen.

10.6 Record the load and extension at the yield point (if one exists) and the load and extension at the moment of rupture.

NOTE 12—If it is desired to measure both modulus and failure properties (yield or break, or both), it may be necessary, in the case of highly extensible materials, to run two independent tests. The high magnification extensometer normally used to determine properties up to the yield point may not be suitable for tests involving high extensibility. If allowed to remain attached to the specimen, the extensometer could be permanently damaged. A broad-range incremental extensometer or hand-rule technique may be needed when such materials are taken to rupture.

11. Calculation

11.1 Toe compensation shall be made in accordance with Annex A1, unless it can be shown that the toe region of the curve is not due to the take-up of slack, seating of the specimen, or other artifact, but rather is an authentic material response.

11.2 *Tensile Strength*—Calculate the tensile strength by dividing the maximum load sustained by the specimen in newtons (pounds-force) by the average original cross-sectional area in the gage length segment of the specimen in square metres (square inches). Express the result in pascals (pounds-force per square inch) and report it to three significant figures as tensile strength at yield or tensile strength at break, whichever term is applicable. When a nominal yield or break load less than the maximum is present and applicable, it is

often desirable to also calculate, in a similar manner, the corresponding tensile stress at yield or tensile stress at break and report it to three significant figures (see Note A2.8).

11.3 Elongation values are valid and are reported in cases where uniformity of deformation within the specimen gage length is present. Elongation values are quantitatively relevant and appropriate for engineering design. When non-uniform deformation (such as necking) occurs within the specimen gage length nominal strain values are reported. Nominal strain values are of qualitative utility only.

11.3.1 *Percent Elongation*—Percent elongation is the change in gage length relative to the original specimen gage length, expressed as a percent. Percent elongation is calculated using the apparatus described in 5.2.

11.3.1.1 *Percent Elongation at Yield*—Calculate the percent elongation at yield by reading the extension (change in gage length) at the yield point. Divide that extension by the original gage length and multiply by 100.

11.3.1.2 *Percent Elongation at Break*—Calculate the percent elongation at break by reading the extension (change in gage length) at the point of specimen rupture. Divide that extension by the original gage length and multiply by 100.

11.3.2 *Nominal Strain*—Nominal strain is the change in grip separation relative to the original grip separation expressed as a percent. Nominal strain is calculated using the apparatus described in 5.1.7.

11.3.2.1 *Nominal strain at break*—Calculate the nominal strain at break by reading the extension (change in grip separation) at the point of rupture. Divide that extension by the original grip separation and multiply by 100.

11.4 *Modulus of Elasticity*—Calculate the modulus of elasticity by extending the initial linear portion of the load-extension curve and dividing the difference in stress corresponding to any segment of section on this straight line by the corresponding difference in strain. All elastic modulus values shall be computed using the average original cross-sectional area in the gage length segment of the specimen in the calculations. The result shall be expressed in pascals (pounds-force per square inch) and reported to three significant figures.

11.5 *Secant Modulus*—At a designated strain, this shall be calculated by dividing the corresponding stress (nominal) by the designated strain. Elastic modulus values are preferable and shall be calculated whenever possible. However, for materials where no proportionality is evident, the secant value shall be calculated. Draw the tangent as directed in A1.3 and Fig. A1.2, and mark off the designated strain from the yield point where the tangent line goes through zero stress. The stress to be used in the calculation is then determined by dividing the load-extension curve by the original average cross-sectional area of the specimen.

11.6 For each series of tests, calculate the arithmetic mean of all values obtained and report it as the “average value” for the particular property in question.

11.7 Calculate the standard deviation (estimated) as follows and report it to two significant figures:

$$s = \sqrt{(\sum X^2 - n\bar{X}^2)/(n-1)} \quad (1)$$

where:

s = estimated standard deviation,
 X = value of single observation,
 n = number of observations, and
 \bar{X} = arithmetic mean of the set of observations.

11.8 See [Annex A1](#) for information on toe compensation.

11.9 See [Annex A3](#) for the determination of Poisson's Ratio.

12. Report

12.1 Report the following information:

12.1.1 Complete identification of the material tested, including type, source, manufacturer's code numbers, form, principal dimensions, previous history, etc.,

12.1.2 Method of preparing test specimens,

12.1.3 Type of test specimen and dimensions,

12.1.4 Conditioning procedure used,

12.1.5 Atmospheric conditions in test room,

12.1.6 Number of specimens tested; for anisotropic materials, the number of specimens tested and the direction in which they were tested,

12.1.7 Speed of testing,

12.1.8 Classification of extensometers used. A description of measuring technique and calculations employed instead of a minimum Class-C extensometer system,

12.1.9 Tensile strength at yield or break, average value, and standard deviation,

12.1.10 Tensile stress at yield or break, if applicable, average value, and standard deviation,

12.1.11 Percent elongation at yield, or break, or nominal strain at break, or all three, as applicable, average value, and standard deviation,

12.1.12 Modulus of elasticity or secant modulus, average value, and standard deviation,

12.1.13 If measured, Poisson's ratio, average value, standard deviation, and statement of whether there was proportionality within the strain range,

12.1.14 Date of test, and

12.1.15 Revision date of Test Method D638.

13. Precision and Bias⁵

13.1 *Precision*—[Tables 2-4](#) are based on a round-robin test conducted in 1984, involving five materials tested by eight laboratories using the Type I specimen, all of nominal 0.125-in. thickness. Each test result was based on five individual determinations. Each laboratory obtained two test results for each material.

⁵ Supporting data are available from ASTM Headquarters. Request RR:D20-1125 for the 1984 round robin and RR:D20-1170 for the 1988 round robin.

TABLE 3 Tensile Stress at Break, 10³ psi, for Eight Laboratories, Five Materials^A

	Mean	S_r	S_R	I_r	I_R
Polypropylene	2.97	1.54	1.65	4.37	4.66
Cellulose acetate butyrate	4.82	0.058	0.180	0.164	0.509
Acrylic	9.09	0.452	0.751	1.27	2.13
Glass-reinforced polyester	20.8	0.233	0.437	0.659	1.24
Glass-reinforced nylon	23.6	0.277	0.698	0.784	1.98

^ATensile strength and elongation at break values obtained for unreinforced propylene plastics generally are highly variable due to inconsistencies in necking or "drawing" of the center section of the test bar. Since tensile strength and elongation at yield are more reproducible and relate in most cases to the practical usefulness of a molded part, they are generally recommended for specification purposes.

TABLE 4 Elongation at Break, %, for Eight Laboratories, Five Materials^A

	Mean	S_r	S_R	I_r	I_R
Glass-reinforced polyester	3.68	0.20	2.33	0.570	6.59
Glass-reinforced nylon	3.87	0.10	2.13	0.283	6.03
Acrylic	13.2	2.05	3.65	5.80	10.3
Cellulose acetate butyrate	14.1	1.87	6.62	5.29	18.7
Polypropylene	293.0	50.9	119.0	144.0	337.0

^ATensile strength and elongation at break values obtained for unreinforced propylene plastics generally are highly variable due to inconsistencies in necking or "drawing" of the center section of the test bar. Since tensile strength and elongation at yield are more reproducible and relate in most cases to the practical usefulness of a molded part, they are generally recommended for specification purposes.

13.1.1 [Tables 5-8](#) are based on a round-robin test conducted by the polyolefin subcommittee in 1988, involving eight polyethylene materials tested in ten laboratories. For each material, all samples were molded at one source, but the individual specimens were prepared at the laboratories that tested them. Each test result was the average of five individual determinations. Each laboratory obtained three test results for each material. Data from some laboratories could not be used for various reasons, and this is noted in each table.

13.1.2 [Tables 9 and 10](#) are based on a round-robin test conducted by the polyolefin subcommittee in 1988, involving three materials tested in eight laboratories. For each material, all samples were molded at one source, but the individual specimens were prepared at the laboratories that tested them. Each test result was the average of five individual determinations. Each laboratory obtained three test results for each material.

TABLE 5 Tensile Yield Stress, for Ten Laboratories, Eight Materials

Material	Test Speed, in./min	Values Expressed in psi Units				
		Average	S_r	S_R	r	R
LDPE	20	1544	52.4	64.0	146.6	179.3
LDPE	20	1894	53.1	61.2	148.7	171.3
LLDPE	20	1879	74.2	99.9	207.8	279.7
LLDPE	20	1791	49.2	75.8	137.9	212.3
LLDPE	20	2900	55.5	87.9	155.4	246.1
LLDPE	20	1730	63.9	96.0	178.9	268.7
HDPE	2	4101	196.1	371.9	549.1	1041.3
HDPE	2	3523	175.9	478.0	492.4	1338.5

TABLE 6 Tensile Yield Elongation, for Eight Laboratories, Eight Materials

Material	Test Speed, in./min	Values Expressed in Percent Units				
		Average	S_r	S_R	r	R
LDPE	20	17.0	1.26	3.16	3.52	8.84
LDPE	20	14.6	1.02	2.38	2.86	6.67
LLDPE	20	15.7	1.37	2.85	3.85	7.97
LLDPE	20	16.6	1.59	3.30	4.46	9.24
LLDPE	20	11.7	1.27	2.88	3.56	8.08
LLDPE	20	15.2	1.27	2.59	3.55	7.25
HDPE	2	9.27	1.40	2.84	3.91	7.94
HDPE	2	9.63	1.23	2.75	3.45	7.71

TABLE 7 Tensile Break Stress, for Nine Laboratories, Six Materials

Material	Test Speed, in./min	Values Expressed in psi Units				
		Average	S_r	S_R	r	R
LDPE	20	1592	52.3	74.9	146.4	209.7
LDPE	20	1750	66.6	102.9	186.4	288.1
LLDPE	20	4379	127.1	219.0	355.8	613.3
LLDPE	20	2840	78.6	143.5	220.2	401.8
LLDPE	20	1679	34.3	47.0	95.96	131.6
LLDPE	20	2660	119.1	166.3	333.6	465.6

TABLE 8 Tensile Break Elongation, for Nine Laboratories, Six Materials

Material	Test Speed, in./min	Values Expressed in Percent Units				
		Average	S_r	S_R	r	R
LDPE	20	567	31.5	59.5	88.2	166.6
LDPE	20	569	61.5	89.2	172.3	249.7
LLDPE	20	890	25.7	113.8	71.9	318.7
LLDPE	20	64.4	6.68	11.7	18.7	32.6
LLDPE	20	803	25.7	104.4	71.9	292.5
LLDPE	20	782	41.6	96.7	116.6	270.8

TABLE 9 Tensile Stress at Yield, 10³ psi, for Eight Laboratories, Three Materials

	Mean	S_r	S_R	I_r	I_R
Polypropylene	3.63	0.022	0.161	0.062	0.456
Cellulose acetate butyrate	5.01	0.058	0.227	0.164	0.642
Acrylic	10.4	0.067	0.317	0.190	0.897

13.1.3 **Table 11** is based on a repeatability study involving a single laboratory. The two materials used were unfilled polypropylene types. Measurements were performed by a single technician on a single day. Each test result is an individual determination. Testing was run using two Type B-1 extensometers for transverse and axial measurements at a test speed of 5 mm/min.

13.1.4 In **Tables 2-11**, for the materials indicated, and for test results that derived from testing five specimens:

TABLE 10 Elongation at Yield, %, for Eight Laboratories, Three Materials

	Mean	S_r	S_R	I_r	I_R
Cellulose acetate butyrate	3.65	0.27	0.62	0.76	1.75
Acrylic	4.89	0.21	0.55	0.59	1.56
Polypropylene	8.79	0.45	5.86	1.27	16.5

TABLE 11 Poisson's Ratio Repeatability Data for One Laboratory and Two Polypropylene Materials

Materials	Values Expressed as a Dimensionless Ratio		
	Average	S_r	r
PP #1 Chord	0.412	0.009	0.026
PP #1 Least Squares	0.413	0.011	0.032
PP #2 Chord	0.391	0.009	0.026
PP #2 Least Squares	0.392	0.010	0.028

13.1.4.1 S_r is the within-laboratory standard deviation of the average; $I_r = 2.83 S_r$. (See **13.1.4.3** for application of I_r .)

13.1.4.2 S_R is the between-laboratory standard deviation of the average; $I_R = 2.83 S_R$. (See **13.1.4.4** for application of I_R .)

13.1.4.3 *Repeatability*—In comparing two test results for the same material, obtained by the same operator using the same equipment on the same day, those test results should be judged not equivalent if they differ by more than the I_r value for that material and condition.

13.1.4.4 *Reproducibility*—In comparing two test results for the same material, obtained by different operators using different equipment on different days, those test results should be judged not equivalent if they differ by more than the I_R value for that material and condition. (This applies between different laboratories or between different equipment within the same laboratory.)

13.1.4.5 Any judgment in accordance with **13.1.4.3** and **13.1.4.4** will have an approximate 95 % (0.95) probability of being correct.

13.1.4.6 Other formulations may give somewhat different results.

13.1.4.7 For further information on the methodology used in this section, see Practice **E691**.

13.1.4.8 The precision of this test method is very dependent upon the uniformity of specimen preparation, standard practices for which are covered in other documents.

13.2 *Bias*—There are no recognized standards on which to base an estimate of bias for this test method.

14. Keywords

14.1 modulus of elasticity; percent elongation; plastics; Poisson's Ratio; tensile properties; tensile strength

ANNEXES

(Mandatory Information)

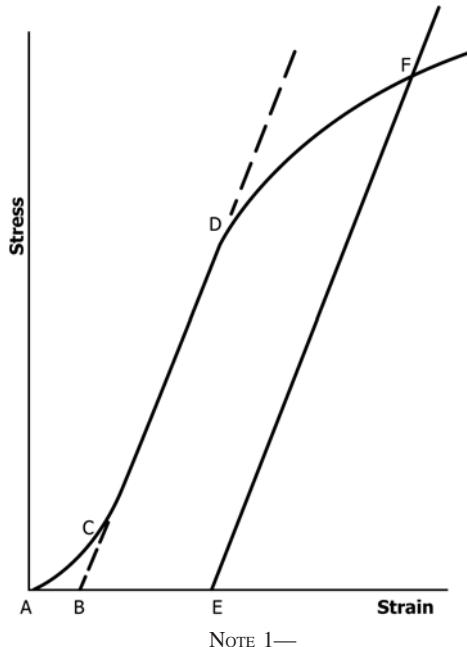
A1. TOE COMPENSATION

A1.1 In a typical stress-strain curve (Fig. A1.1) there is a toe region, AC, that does not represent a property of the material. It is an artifact caused by a takeup of slack and alignment or seating of the specimen. In order to obtain correct values of such parameters as modulus, strain, and offset yield point, this artifact must be compensated for to give the corrected zero point on the strain or extension axis.

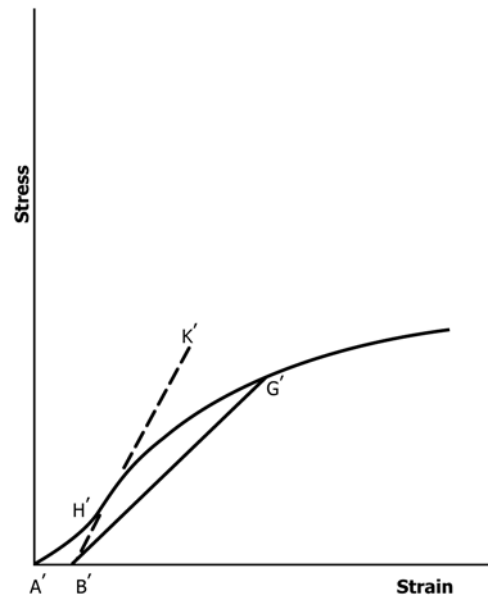
A1.2 In the case of a material exhibiting a region of Hookean (linear) behavior (Fig. A1.1), a continuation of the linear (CD) region of the curve is constructed through the zero-stress axis. This intersection (B) is the corrected zero-strain point from which all extensions or strains must be measured, including the yield offset (BE), if applicable. The

elastic modulus can be determined by dividing the stress at any point along the line CD (or its extension) by the strain at the same point (measured from Point B, defined as zero-strain).

A1.3 In the case of a material that does not exhibit any linear region (Fig. A1.2), the same kind of toe correction of the zero-strain point can be made by constructing a tangent to the maximum slope at the inflection point (H'). This is extended to intersect the strain axis at Point B', the corrected zero-strain point. Using Point B' as zero strain, the stress at any point (G') on the curve can be divided by the strain at that point to obtain a secant modulus (slope of Line B'G'). For those materials with no linear region, any attempt to use the tangent through the inflection point as a basis for determination of an offset yield point may result in unacceptable error.



NOTE 1—
Some chart recorders plot the mirror image of this graph.
FIG. A1.1 Material with Hookean Region



NOTE 1—Some chart recorders plot the mirror image of this graph.
FIG. A1.2 Material with No Hookean Region

A2. DEFINITIONS OF TERMS AND SYMBOLS RELATING TO TENSION TESTING OF PLASTICS

A2.1 elastic limit—the greatest stress which a material is capable of sustaining without any permanent strain remaining upon complete release of the stress. It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

NOTE A2.1—Measured values of proportional limit and elastic limit vary greatly with the sensitivity and accuracy of the testing equipment, eccentricity of loading, the scale to which the stress-strain diagram is plotted, and other factors. Consequently, these values are usually replaced by yield strength.

A2.2 elongation—the increase in length produced in the gage length of the test specimen by a tensile load. It is expressed in units of length, usually millimetres (inches). (Also known as *extension*.)

NOTE A2.2—Elongation and strain values are valid only in cases where uniformity of specimen behavior within the gage length is present. In the case of materials exhibiting necking phenomena, such values are only of qualitative utility after attainment of yield point. This is due to inability to ensure that necking will encompass the entire length between the gage marks prior to specimen failure.

A2.3 gage length—the original length of that portion of the specimen over which strain or change in length is determined.

A2.4 modulus of elasticity—the ratio of stress (nominal) to corresponding strain below the proportional limit of a material. It is expressed in force per unit area, usually megapascals (pounds-force per square inch). (Also known as *elastic modulus* or *Young's modulus*).

NOTE A2.3—The stress-strain relations of many plastics do not conform to Hooke's law throughout the elastic range but deviate therefrom even at stresses well below the elastic limit. For such materials the slope of the tangent to the stress-strain curve at a low stress is usually taken as the modulus of elasticity. Since the existence of a true proportional limit in plastics is debatable, the propriety of applying the term "modulus of elasticity" to describe the stiffness or rigidity of a plastic has been seriously questioned. The exact stress-strain characteristics of plastic materials are very dependent on such factors as rate of stressing, temperature, previous specimen history, etc. However, such a value is useful if its arbitrary nature and dependence on time, temperature, and other factors are realized.

A2.5 necking—the localized reduction in cross section which may occur in a material under tensile stress.

A2.6 offset yield strength—the stress at which the strain exceeds by a specified amount (the offset) an extension of the initial proportional portion of the stress-strain curve. It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

NOTE A2.4—This measurement is useful for materials whose stress-strain curve in the yield range is of gradual curvature. The offset yield strength can be derived from a stress-strain curve as follows (Fig. A2.1):

On the strain axis lay off OM equal to the specified offset. Draw OA tangent to the initial straight-line portion of the stress-strain curve.

Through M draw a line MN parallel to OA and locate the intersection of MN with the stress-strain curve.

The stress at the point of intersection r is the "offset yield strength." The specified value of the offset must be stated as a percent of the original gage length in conjunction with the strength value. *Example:* 0.1 % offset yield strength = ... MPa (psi), or yield strength at 0.1 % offset ... MPa (psi).

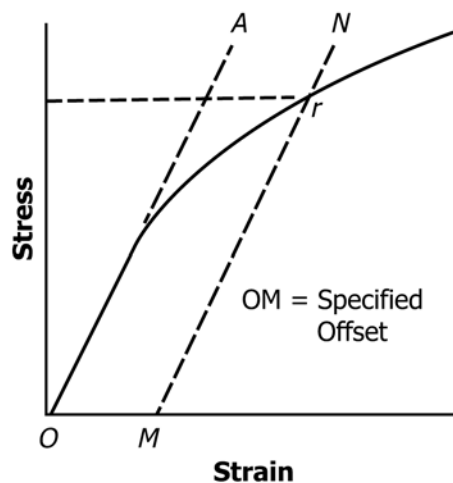


FIG. A2.1 Offset Yield Strength

A2.7 percent elongation—the elongation of a test specimen expressed as a percent of the gage length.

A2.8 percent elongation at break and yield:

A2.8.1 percent elongation at break—the percent elongation at the moment of rupture of the test specimen.

A2.8.2 percent elongation at yield—the percent elongation at the moment the yield point (A2.22) is attained in the test specimen.

A2.9 percent reduction of area (nominal)—the difference between the original cross-sectional area measured at the point of rupture after breaking and after all retraction has ceased, expressed as a percent of the original area.

A2.10 percent reduction of area (true)—the difference between the original cross-sectional area of the test specimen and the minimum cross-sectional area within the gage boundaries prevailing at the moment of rupture, expressed as a percentage of the original area.

A2.11 Poisson's Ratio—The absolute value of the ratio of transverse strain to the corresponding axial strain resulting from uniformly distributed axial stress below the proportional limit of the material.

A2.12 proportional limit—the greatest stress which a material is capable of sustaining without any deviation from proportionality of stress to strain (Hooke's law). It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

A2.13 rate of loading—the change in tensile load carried by the specimen per unit time. It is expressed in force per unit time, usually newtons (pounds-force) per minute. The initial rate of loading can be calculated from the initial slope of the load versus time diagram.

A2.14 rate of straining—the change in tensile strain per unit time. It is expressed either as strain per unit time, usually metres per metre (inches per inch) per minute, or percent elongation per unit time, usually percent elongation per minute. The initial rate of straining can be calculated from the initial slope of the tensile strain versus time diagram.

NOTE A2.5—The initial rate of straining is synonymous with the rate of crosshead movement divided by the initial distance between crossheads only in a machine with constant rate of crosshead movement and when the specimen has a uniform original cross section, does not “neck down,” and does not slip in the jaws.

A2.15 rate of stressing (nominal)—the change in tensile stress (nominal) per unit time. It is expressed in force per unit area per unit time, usually megapascals (pounds-force per square inch) per minute. The initial rate of stressing can be calculated from the initial slope of the tensile stress (nominal) versus time diagram.

NOTE A2.6—The initial rate of stressing as determined in this manner has only limited physical significance. It does, however, roughly describe the average rate at which the initial stress (nominal) carried by the test specimen is applied. It is affected by the elasticity and flow characteristics of the materials being tested. At the yield point, the rate of stressing (true) may continue to have a positive value if the cross-sectional area is decreasing.

A2.16 secant modulus—the ratio of stress (nominal) to corresponding strain at any specified point on the stress-strain curve. It is expressed in force per unit area, usually megapascals (pounds-force per square inch), and reported together with the specified stress or strain.

NOTE A2.7—This measurement is usually employed in place of modulus of elasticity in the case of materials whose stress-strain diagram does not demonstrate proportionality of stress to strain.

A2.17 strain—the ratio of the elongation to the gage length of the test specimen, that is, the change in length per unit of original length. It is expressed as a dimensionless ratio.

A2.17.1 nominal strain at break—the strain at the moment of rupture relative to the original grip separation.

A2.18 tensile strength (nominal)—the maximum tensile stress (nominal) sustained by the specimen during a tension test. When the maximum stress occurs at the yield point (A2.22), it shall be designated tensile strength at yield. When the maximum stress occurs at break, it shall be designated tensile strength at break.

A2.19 tensile stress (nominal)—the tensile load per unit area of minimum original cross section, within the gage boundaries, carried by the test specimen at any given moment.

It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

NOTE A2.8—The expression of tensile properties in terms of the minimum original cross section is almost universally used in practice. In the case of materials exhibiting high extensibility or necking, or both (A2.16), nominal stress calculations may not be meaningful beyond the yield point (A2.22) due to the extensive reduction in cross-sectional area that ensues. Under some circumstances it may be desirable to express the tensile properties per unit of minimum prevailing cross section. These properties are called true tensile properties (that is, true tensile stress, etc.).

A2.20 tensile stress-strain curve—a diagram in which values of tensile stress are plotted as ordinates against corresponding values of tensile strain as abscissas.

A2.21 true strain (see Fig. A2.2) is defined by the following equation for ϵ_T :

$$\epsilon_T = \int_{L_o}^L dL/L = \ln L/L_o \quad (\text{A2.1})$$

where:

dL = increment of elongation when the distance between the gage marks is L ,

L_o = original distance between gauge marks, and

L = distance between gauge marks at any time.

A2.22 yield point—the first point on the stress-strain curve at which an increase in strain occurs without an increase in stress (Fig. A2.2).

NOTE A2.9—Only materials whose stress-strain curves exhibit a point of zero slope may be considered as having a yield point.

NOTE A2.10—Some materials exhibit a distinct “break” or discontinuity in the stress-strain curve in the elastic region. This break is not a yield point by definition. However, this point may prove useful for material characterization in some cases.

A2.23 yield strength—the stress at which a material exhibits a specified limiting deviation from the proportionality of stress to strain. Unless otherwise specified, this stress will be the stress at the yield point and when expressed in relation to the tensile strength shall be designated either tensile strength at yield or tensile stress at yield as required in A2.18 (Fig. A2.3). (See *offset yield strength*.)

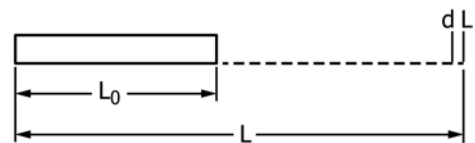


FIG. A2.2 Illustration of True Strain Equation

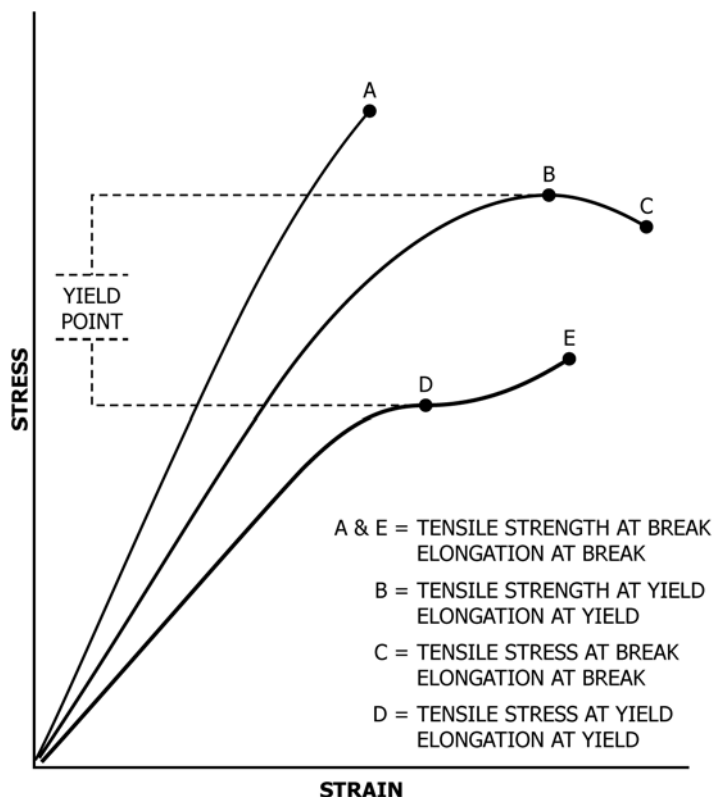


FIG. A2.3 Tensile Designations

A2.24 *Symbols*—The following symbols may be used for the above terms:

Symbol	Term
W	Load
ΔW	Increment of load
L	Distance between gage marks at any time
L_o	Original distance between gage marks
L_u	Distance between gage marks at moment of rupture
ΔL	Increment of distance between gage marks = elongation

A	Minimum cross-sectional area at any time
A_o	Original cross-sectional area
ΔA	Increment of cross-sectional area
A_u	Cross-sectional area at point of rupture measured after breaking specimen
A_T	Cross-sectional area at point of rupture, measured at the moment of rupture
t	Time
Δt	Increment of time
σ	Tensile stress
$\Delta \sigma$	Increment of stress
σ_T	True tensile stress
σ_U	Tensile strength at break (nominal)
σ_{UT}	Tensile strength at break (true)
ϵ	Strain
$\Delta \epsilon$	Increment of strain
ϵ_U	Total strain, at break
ϵ_T	True strain
$\%EI$	Percentage elongation
Y.P.	Yield point
E	Modulus of elasticity

A2.25 Relations between these various terms may be defined as follows:

$$\begin{aligned}\sigma &= W/A_o \\ \sigma_T &= W/A \\ \sigma_U &= W/A_o \text{ (where } W \text{ is breaking load)} \\ \sigma_{UT} &= W/A_T \text{ (where } W \text{ is breaking load)} \\ \epsilon &= \Delta L/L_o = (L - L_o)/L_o \\ \epsilon_U &= (L_u - L_o)/L_o \\ \epsilon_T &= \int_{L_o}^L dL/L = \ln L/L_o \\ \%EI &= [(L - L_o)/L_o] \times 100 = \epsilon \times 100\end{aligned}$$

Percent reduction of area (nominal) = $[(A_o - A_u)/A_o] \times 100$

Percent reduction of area (true) = $[(A_o - A_T)/A_o] \times 100$

Rate of loading = $\Delta W/\Delta t$

Rate of stressing (nominal) = $\Delta \sigma/\Delta = (\Delta W)/A_o/\Delta t$

Rate of straining = $\Delta \epsilon/\Delta t = (\Delta L/L_o)\Delta t$

For the case where the volume of the test specimen does not change during the test, the following three relations hold:

$$\sigma_T = \sigma(1 + \epsilon) = \sigma L/L_o \quad (A2.2)$$

$$\sigma_{UT} = \sigma_U(1 + \epsilon_U) = \sigma_U L_u/L_o$$

$$A = A_o/(1 + \epsilon)$$

A3. MEASUREMENT OF POISSON'S RATIO

A3.1. Scope

A3.1.1 This test method covers the determination of Poisson's ratio obtained from strains resulting from uniaxial stress only.

A3.1.2 Test data obtained by this test method are relevant and appropriate for use in engineering design.

A3.1.3 The values stated in SI units are regarded as the standard. The values given in parentheses are for information only.

NOTE A3.1—This standard is not equivalent to ISO 527-1.

A3.2. Referenced Documents

A3.2.1 *ASTM Standards*:²

D618 Practice for Conditioning Plastics for Testing

D883 Terminology Relating to Plastics

D5947 Test Methods for Physical Dimensions of Solid Plastics Specimens

E83 Practice for Verification and Classification of Extensometer Systems

E132 Test Method for Poisson's Ratio at Room Temperature

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

E1012 Practice for Verification of Testing Frame and Specimen Alignment Under Tensile and Compressive Axial Force Application

A3.2.2 ISO Standard:⁴

ISO 527-1 Determination of Tensile Properties

A3.3. Terminology

A3.3.1 *Definitions*—Definitions of terms applying to this test method appear in Terminology D883 and Annex A2 of this standard.

A3.4. Significance and Use

A3.4.1 When uniaxial tensile force is applied to a solid, the solid stretches in the direction of the applied force (axially), but it also contracts in both dimensions perpendicular to the applied force. If the solid is homogeneous and isotropic, and the material remains elastic under the action of the applied force, the transverse strain bears a constant relationship to the axial strain. This constant, called Poisson's ratio, is defined as the negative ratio of the transverse (negative) to axial strain under uniaxial stress.

A3.4.2 Poisson's ratio is used for the design of structures in which all dimensional changes resulting from the application of force need to be taken into account and in the application of the generalized theory of elasticity to structural analysis.

NOTE A3.2—The accuracy of the determination of Poisson's ratio is usually limited by the accuracy of the transverse strain measurements because the percentage errors in these measurements are usually greater than in the axial strain measurements. Since a ratio rather than an absolute quantity is measured, it is only necessary to know accurately the relative value of the calibration factors of the extensometers. Also, in general, the value of the applied loads need not be known accurately.

A3.5. Apparatus

A3.5.1 Refer to 5.1 and 5.3 of this standard for the requirements of the testing machine and micrometers.

A3.5.2 For measurement of Poisson's Ratio use either a bi-axial extensometer or an axial extensometer in combination with a transverse extensometer. They must be capable of recording axial strain and transverse strain simultaneously. The extensometers shall be capable of measuring the change in strains with an accuracy of 1 % of the relevant value or better.

NOTE A3.3—Strain gages are used as an alternative method to measure axial and transverse strain; however, proper techniques for mounting strain gauges are crucial to obtaining accurate data. Consult strain gauge suppliers for instruction and training in these special techniques.

A3.6. Test Specimen

A3.6.1 *Specimen*—The test specimen shall conform to the dimensions shown in Fig. 1. The Type I specimen is the preferred specimen and shall be used where sufficient material having a thickness of 7 mm (0.28 in.) or less is available.

A3.6.2 *Preparation*—Test specimens shall be prepared by machining operations, or die cutting, from materials in sheet, plate, slab, or similar form or be prepared by molding the material into the specimen shape to be tested.

NOTE A3.4—When preparing specimens from certain composite laminates such as woven roving, or glass cloth, care must be exercised in

cutting the specimens parallel to the reinforcement, unless testing of specimens in a direction other than parallel with the reinforcement constitutes a variable being studied.

NOTE A3.5—Specimens prepared by injection molding have different tensile properties than specimens prepared by machining or die-cutting because of the orientation induced. This effect is more pronounced in specimens with narrow sections.

A3.6.3 All surfaces of the specimen shall be free of visible flaws, scratches, or imperfections. Marks left by coarse machining operations shall be carefully removed with a fine file or abrasive, and the filed surfaces shall then be smoothed with abrasive paper (No. 00 or finer). The finishing sanding strokes shall be made in a direction parallel to the long axis of the test specimen. All flash shall be removed from a molded specimen, taking great care not to disturb the molded surfaces. In machining a specimen, undercuts that would exceed the dimensional tolerances shown in Fig. 1 shall be scrupulously avoided. Care shall also be taken to avoid other common machining errors.

A3.6.4 If it is necessary to place gage marks on the specimen, this shall be done with a wax crayon or India ink that will not affect the material being tested. Gauge marks shall not be scratched, punched, or impressed on the specimen.

A3.6.5 When testing materials that are suspected of anisotropy, duplicate sets of test specimens shall be prepared, having their long axes respectively parallel with, and normal to, the suspected direction of anisotropy.

A3.7. Number of Test Specimens

A3.7.1 Test at least five specimens for each sample in the case of isotropic materials.

A3.7.2 Test ten specimens, five normal to, and five parallel with, the principle axis of anisotropy, for each sample in the case of anisotropic materials.

A3.8. Conditioning

A3.8.1 Specimens shall be conditioned and tested in accordance with the requirement shown in Section 9 of this standard.

A3.9. Procedure

A3.9.1 Measure the width and thickness of each specimen to the nearest 0.025 mm (0.001 in.) using the applicable test methods in D5947. Follow the guidelines specified in 10.1.1 and 10.1.2 of this standard.

A3.9.2 Poisson's Ratio shall be determined at a speed of 5 mm/min.

A3.9.3 Place the specimen in the grips of the testing machine, taking care to align the long axis of the specimen and the grips with an imaginary line joining the points of attachment of the grips to the machine. The distance between the ends of the gripping surfaces, when using flat specimens, shall be as indicated in Fig. 1. Tighten the grips evenly and firmly to the degree necessary to prevent slippage of the specimen during the test, but not to the point where the specimen would be crushed.

A3.9.4 Attach the biaxial extensometer or the axial and transverse extensometer combination to the specimen. The transverse extensometer should be attached to the width of the specimen.

A3.9.5 Apply a small preload (less than 5 N) to the specimen at a crosshead speed of 0.1 mm/min. This preload will eliminate any bending in the specimens.

A3.9.6 Rebalance the extensometers to zero.

A3.9.7 Run the test at 5 mm/min out to a minimum of 0.5 % strain before removing the extensometers, simultaneously recording the strain readings from the extensometers at the same applied force. The precision of the value of Poisson's Ratio will depend on the number of data points of axial and transverse strain taken. It is recommended that the data collection rate for the test be a minimum of 20 points per second (but preferably higher). This is particularly important for materials having a non linear stress to strain curve.

A3.9.8 Make the toe compensation in accordance with **Annex A1**. Determine the maximum strain (proportional limit) at which the curve is linear. If this strain is greater than 0.25 % the Poisson's Ratio is to be determined anywhere in this linear portion of the curve below the proportional limit. If the material does not exhibit a linear stress to strain relationship the Poisson's Ratio shall be determined within the axial strain range of 0.0005 to 0.0025 mm/mm (0.05 to 0.25 %). If the ratio is determined in this manner it shall be noted in the report that a region of proportionality of stress to strain was not evident.

NOTE A3.6—A suitable method for determination of linearity of the stress to strain curve is by making a series of tangent modulus measurements at different axial strain levels. Values equivalent at each strain level indicate linearity. Values showing a downward trend with increasing strain level indicate non linearity.

A3.10. Calculation

A3.10.1 *Poisson's Ratio*—The axial strain, ϵ_a , indicated by the axial extensometer, and the transverse strain, ϵ_t , indicated by the transverse extensometers, are plotted against the applied load, P , as shown in **Fig. A3.1**.

A3.10.1.1 For those materials where there is proportionality of stress to strain and it is possible to determine a modulus of elasticity, a straight line is drawn through each set of points within the load range used for determination of modulus, and the slopes $d\epsilon_a / dP$ and $d\epsilon_t / dP$, of those lines are determined. The use of a least squares method of calculation will reduce errors resulting from drawing lines. Poisson's Ratio, $|\mu|$, is then calculated as follows:

$$|\mu| = (d\epsilon_t / dP) / (d\epsilon_a / dP) \quad (A3.1)$$

where:

$d\epsilon_t$ = change in transverse strain,

$d\epsilon_a$ = change in axial strain, and

dP = change in applied load;

$$|\mu| = (d\epsilon_t) / (d\epsilon_a) \quad (A3.2)$$

A3.10.1.2 The errors that are introduced by drawing a straight line through the points are reduced by applying the least squares method.

A3.10.1.3 For those materials where there is no proportionality of stress to strain evident determine the ratio of $d\epsilon_t / d\epsilon_a$ when $d\epsilon_a = 0.002$ (based on axial strain range of 0.0005 to 0.0025 mm/mm) and after toe compensation has been made.

$$|\mu| = (d\epsilon_t) / 0.002 \quad (A3.3)$$

A3.11. Report

A3.11.1 Report the following information:

A3.11.1.1 Complete identification of the material tested, including type, source, manufacturer's code numbers, form, principal dimensions, previous history, etc.,

A3.11.1.2 Method of preparing test specimens,

A3.11.1.3 Type of test specimen and dimensions,

A3.11.1.4 Conditioning procedure used,

A3.11.1.5 Atmospheric conditions in test room,

A3.11.1.6 Number of specimens tested,

A3.11.1.7 Speed of testing,

A3.11.1.8 Classification of extensometers used. A description of measuring technique and calculations employed,

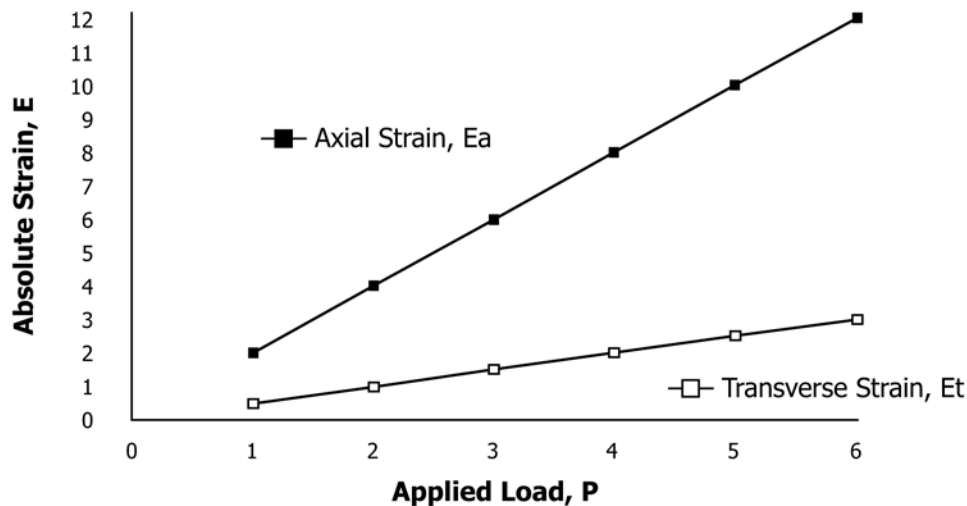


FIG. A3.1 Plot of Strains Versus Load for Determination of Poisson's Ratio



A3.11.1.9 Poisson's ratio, average value, standard deviation, and statement of whether there was proportionality within the strain range,

A3.11.1.10 Date of test, and

A3.11.1.11 Revision date of Test Method **D618**.

A3.12. Precision and Bias

A3.12.1 *Precision*—The repeatability standard deviation has been determined to be the following (see **Table A3.1**.) An attempt to develop a full precision and bias statement for this test method will be made at a later date. For this reason, data

on precision and bias cannot be given. Because this test method does not contain a round-robin based numerical precision and bias statement, it shall not be used as a referee test method in case of dispute. Anyone wishing to participate in the development of precision and bias data should contact the Chairman, Subcommittee D20.10 Mechanical Properties, ASTM International, 100 Barr Harbor, West Conshohocken, PA 19428.

A3.13 Keywords

axial strain; Poisson's ratio; transverse strain

TABLE A3.1 Poisson's Ratio Based on One Laboratory

Material	Extensometer Type	Average	V_r^A	V_R^B	r^C	R^D
PP Copolymer	2-point	0.408	0.011		0.031	
PP Copolymer	4-point	0.392	0.010		0.028	
PP Homopolymer with 20 % Glass	2-point	0.428	0.013		0.036	
PP Homopolymer with 20 % Glass	4-point	0.410	0.015		0.042	

^A S_r = within laboratory standard deviation for the indicated material. It is obtained by first pooling the with-laboratory standard deviations of the test results from all the participating laboratories:

$$S_r = \{[(S_1)^2 + (S_2)^2 + \dots + (S_n)^2]/n\}^{1/2}$$

^B S_R = between-laboratories reproducibility, expressed as standard deviation: $S_R = [S_r^2 + S_L^2]^{1/2}$

^C r = within-laboratory critical interval between two test results = $2.8 \times S_r$

^D R = between-laboratories critical interval between two test results = $2.8 \times S_R$

SUMMARY OF CHANGES

Committee D20 has identified the location of selected changes to this standard since the last issue (D638 - 10) that may impact the use of this standard. (December 15, 2014)

- | | |
|---|---|
| <p>(1) Revised Note 1 since changes were made to ISO 527-1, and it is no longer equivalent to this standard.</p> <p>(2) Removed permissive language.</p> | <p>(3) Made some editorial changes.</p> <p>(4) Moved Tables 2-5 to Section 13 on Precision and Bias.</p> <p>(5) Revised Summary of Changes section.</p> |
|---|---|

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Designation: D1076 – 21

Standard Specification for Rubber—Concentrated, Ammonia Stabilized, Creamed, and Centrifuged Natural Latex¹

This standard is issued under the fixed designation D1076; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This specification covers requirements for first grade concentrated natural rubber latex (see [Table 1](#)) of the following categories:

Category 1—Centrifuged *Hevea* natural latex stabilized with ammonia only.

Category 2—Creamed *Hevea* natural latex stabilized with ammonia only.

Category 3—Centrifuged *Hevea* natural latex stabilized with low ammonia.

Category 4—Centrifuged, or centrifuged and creamed, guayule latex, or other natural rubber latex, containing less than 200 μg total protein per gram dry weight of latex, with ammonia or other hydroxide.

Category 5—Centrifuged *Hevea* natural latex treated with aluminum hydroxide or by other means, stabilized with ammonia only containing less than 0.5 % non-rubber content.

1.2 This specification is not necessarily applicable to latices prepared, stabilized, or preserved by other methods, and shall not be construed as limiting the desirability or usefulness of other categories of latices. It does apply to natural latex sources other than *Hevea brasiliensis* but does not apply to compounded latex concentrates.

1.3 The analytical procedures applicable to the specifications are included and appear in the following order:

	Section
Sampling	6 and 7
Total Solids	8
Dry Rubber Content	9
Protein Content	10
Total Alkalinity	11
Viscosity	12
Sludge Content	13
Coagulum Content	14
KOH Number	15
pH	16
Mechanical Stability	17
Copper and Manganese	18

Density	19 – 31
Volatile Fatty Acids	32 – 36
Boric Acid	37
Dry Films	38
Precision for All Test Methods	39

1.4 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 *ASTM Standards*:²

[D1278](#) Test Methods for Rubber from Natural Sources—Chemical Analysis

[D4483](#) Practice for Evaluating Precision for Test Method Standards in the Rubber and Carbon Black Manufacturing Industries

[D5712](#) Test Method for Analysis of Aqueous Extractable Protein in Latex, Natural Rubber, and Elastomeric Products Using the Modified Lowry Method

[D6499](#) Test Method for Immunological Measurement of Antigenic Protein in *Hevea* Natural Rubber (HNR) and its Products

[E70](#) Test Method for pH of Aqueous Solutions With the Glass Electrode

3. General Specification Requirements

3.1 In manufacturing, the material shall be processed in accordance with the best commercial practice and shall be of uniform composition.

3.2 The material shall conform to the chemical and physical requirements prescribed in [Table 1](#).

¹ This specification is under the jurisdiction of ASTM Committee D11 on Rubber and Rubber-like Materials and is the direct responsibility of Subcommittee D11.22 on Natural Rubber.

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

TABLE 1 Requirements for Specified Latex Categories

	Category 1	Category 2	Category 3	Category 4	Category 5
Total solids, min, %	61.3	66.0	61.3	44.0	61.3
Dry rubber content (DRC), ^A min, %	59.8	64.0	59.8	42.0	60.8
Total solids content minus dry rubber content, max, %	2.0	2.0	2.0	2.0	0.5
Protein content (µg/g dw latex)					
Total protein by D5712				200 max	
<i>Hevea</i> antigenic protein by D6499				None detectable	
Total alkalinity calculated as ammonia, as % latex	0.60 min	0.55 min	0.29 max	0.60 min	0.60 min
Or: total alkalinity calculated as KOH, as % latex				0.10 min	
Sludge content, max, %	0.10	0.10	0.10	0.10	0.1
Coagulum content, max, %	0.050	0.050	0.050	0.050	0.05
KOH number, max ^B	0.80	0.80	0.80	0.80	0.8
Mechanical stability, s, min	650	650	650	90	650
Copper content, max, % of total solids	0.0008	0.0008	0.0008	0.0008	0.0008
Manganese content, max, % of total solids	0.0008	0.0008	0.0008	0.0008	0.0008
Color on visual inspection	no pronounced blue or gray ^C				
Odor after neutralization with boric acid	no putrefactive odor				

^A Dry rubber content by definition and use is the acid coagulable portion of latex after washing and drying.

^B It is accepted that KOH numbers for boric acid preserved latices will be higher than normal, equivalent to the amount of boric acid in the latex.

^C Blue or gray color usually denotes iron contamination caused by improper storage in containers.

4. Significance and Use

4.1 This specification denotes limits on the 5 categories of latex as defined in the scope and defines the test methods to use for the specified properties. These test methods may be used for production control or for referee purposes.

5. Inspection

5.1 Inspection of the material shall be made as agreed upon between the purchaser and the seller as part of the purchase contract.

SAMPLING AND METHODS OF TESTING

6. Preparations for Sampling

6.1 Drums:

6.1.1 *Open-Head Drums*—The top shall be removed and the contents stirred with a high-speed stirrer for 10 min.

6.1.2 *Closed-Head Drums*—If the drum has at least 2 % air space, which is 20 mm (0.75 in.) on a standard drum, lay it on its side and roll for not less than 10 min. Up end the drum to its original position and allow to stand for 15 min and then repeat the rolling operation for at least a further 10 min. In the case of drums with less than 2 % air space, all of the latex in the closed-head drum shall be transferred to a larger vessel and mixed with a high-speed stirrer for 10 min.

6.2 *Tank Cars/Tank Trucks*—Samples shall be taken from the top and bottom of the car/truck. If the total solids in the top and bottom samples agree within 0.5 %, the car shall be considered uniform enough for sampling. If top and bottom samples do not agree within 0.5 %, the contents of the car shall be agitated until samples taken from the top and bottom do agree on total solids within 0.5 %.

7. Sampling

7.1 *Drums*—After preparations for sampling, sample without delay. A suitable method is by slowly inserting a clean, dry

glass tube of 10 to 15 mm internal diameter and open at both ends, until it reaches the bottom of the container. Then close the upper end of the tube and transfer the contents to a clean, dry sample bottle. Repeat the operation until sufficient latex has been obtained. Alternatively, a specially constructed metal sampling tube may be used, the bottom of which can be closed by remote control. No copper or brass shall be used in any part of its construction. At least 10 % of the drums in a shipment shall be sampled.

7.2 *Tank Cars/Tank Trucks*—Separate samples of at least 475 cm³ each shall be taken from the top, center, and bottom of the tank car/tank truck. Take the top sample first, then the center sample, and the bottom sample last. Use a weighted sampler with a remotely operated removable top, or other suitable sampling device that will accomplish the same results. Blend the three samples thoroughly. Each sample shall be poured immediately into a tightly stoppered container. The three samples shall be combined and thoroughly blended into a composite sample. At least 950 cm³ of this composite sample shall be used for test. One composite sample only is required from each tank car/tank truck.

8. Total Solids

8.1 *Apparatus*—Tared, covered, flat-bottom weighing dish approximately 60 mm (2.5 in.) in diameter, which may be made of glass, tinned metal, or aluminum.

8.2 *Reagent*—Distilled water.

8.3 *Procedure*—Weigh 2.5 ± 0.5 g of the latex to the nearest 1 mg in the tared, covered weighing dish. Remove the cover and distribute the latex over the bottom of the dish over an area of approximately 32 cm² (5 in.²). This may be facilitated by carefully adding approximately 1 cm³ of distilled water to the latex and gently swirling the dish. With the dish uncovered, dry the specimen in a vented air oven for 16 h at $70 \pm 2^\circ\text{C}$ or 2 h at $100 \pm 2^\circ\text{C}$. Replace the cover, cool in a desiccator to room

temperature, and weigh. Repeat drying and weighing until the mass is constant to 1 mg or less. Tests shall be run in duplicate and shall check within 0.15 %. The average of the two determinations shall be taken as the result.

8.4 *Calculations*—Calculate the percentage of total solids as follows:

$$\text{Total solids, \%} = [(C - A)/(B - A)] \times 100 \quad (1)$$

where:

- A = mass of the weighing dish, g,
- B = mass of the dish plus the original sample, g, and
- C = mass of the dish plus the dried sample, g.

9. Dry Rubber Content

9.1 *Apparatus*—Porcelain evaporating dish approximately 100 mm in diameter and 50 mm deep.

9.2 *Reagent*—Acetic acid aqueous solution (20 Mg/m³).

9.3 Weigh approximately 10 g of the latex to the nearest 1 mg into a porcelain evaporating dish, and add distilled water until the total solids content is approximately 25 %. Add sufficient acetic acid (2 %), while stirring constantly over a 5-min period, to coagulate completely the latex (80 cm³ should be sufficient). Category 4 guayule latex may also require the addition of up to 20 mL hydrochloric acid (2 %) to complete its coagulation.

9.3.1 Place the dish on a steam bath and leave undisturbed for 15 to 30 min. A clear serum should result, and 30 min is the maximum time allowed. If the serum is milky, the acid was either added too fast or in insufficient amount and the procedure should be repeated until a clear serum results. Pick up coagulated latex particles with the main body of the coagulum. Wash coagulum in running water and pass between rolls. Repeat this process 5 times and reduce the sheet of coagulated rubber to a maximum thickness of 2 mm and dry at 70 ± 2°C in a vented air oven atmosphere. If oxidation occurs, the test may be run with the option of using a drying temperature of 55 ± 2°C, or an antioxidant may be added to the latex before coagulation. If polymer oxidation occurs, the test may be rerun with the option of using a drying temperature of 55 ± 2°C. Cool in a desiccator to room temperature and weigh. Repeat drying and weighing until the mass is constant to 1 mg or less.

9.4 Duplicate samples shall be run and shall check within 0.2 %. The average of the two determinations shall be taken as the result.

9.5 *Calculation*—Calculate the dry rubber content as follows:

$$\text{Dry rubber content, \%} = \text{mass of dry coagulum/mass of sample} \times 100 \quad (2)$$

10. Protein Content

10.1 *Total Protein*—Solubilize latex proteins in 1 % SDS and 50 mM sodium phosphate buffer (final concentration) and then quantify using the modified Lowry test according to Test Method D5712.

10.1.1 *Solubilization Method*—Mix latex sample (500 µl) with 450 µl 100 mM sodium phosphate buffer (1:1) into three microfuge tubes for each sample; add 50 µl 20 % SDS into

each tube, mix; incubate at 25°C for 2 h with shaking at 200 rpm; spin for 5 min, remove rubber pad; transfer aqueous phase into new tubes and spin again to clarify; divide each sample into 3 × 0.6 mL tubes for each sample (these can be stored at 4°C overnight); prepare bovine serum albumin standards in extraction buffer at 0, 5, 10, 15, 25, 50, 100, 200, 300, and 400 µg/mL; add 60 µl 1.5 mg/mL sodium deoxycholate to samples and standards, mix, stand for 10 min; add 120 µl of 72 % freshly mixed trichloroacetic acid and phosphotungstic acid (1:1) into each sample, mix, incubate for 30 min at RT; spin 15 min at 6000 xg, remove supernatant, air dry pellet; suspend each pellet in 250 µl 0.2 M sodium hydroxide and store at 4°C until assayed; assay within 24 h using the modified Lowry test according to Test Method D5712.

10.2 *Hevea Antigenic Protein*—Solubilize latex proteins with 1 % SDS and 50 mM sodium phosphate buffer (final concentration) then quantify using the antigenic protein assay according to Test Method D6499.

11. Total Alkalinity

11.1 *Apparatus*—Glass electrode pH meter.

11.2 *Reagent*—0.1 mol standard HCl.

11.3 *Preparation of Specimen*—Place approximately 5 g of latex into a glass weighing bottle of approximately 10-cm³ capacity, having a ground glass cap, and weigh to the nearest 1 mg. Pour the specimen into a beaker containing approximately 300 cm³ of distilled water, restopper quickly to prevent loss of ammonia, and set aside for reweighing. The specimen mass is equal to the difference between the two weighings. The transfer of the sample to the beaker shall be done in such a way that no latex runs down the outside of the weighing bottle.

11.4 *Recommended Procedure*—Insert the electrodes of a calibrated glass electrode pH meter into the liquid and note the pH. The meter should be calibrated and the pH measurements made in accordance with Test Method E70, and the directions given by the manufacturer of the meter. Slowly, and while stirring constantly, add 0.1 mol HCl until a pH of 6.0 is reached. Too rapid addition or inadequate stirring of the sample while the acid is being added may cause local coagulation of the rubber. With samples of unknown alkalinity, it is recommended that the acid be added in 1-cm³ increments, and a pH reading taken 10 s after each addition. As the pH of 6.0 is approached, smaller increments should be added.

11.5 *Alternative Procedure*—Prepare the sample as described in 11.3. Add 6 drops of a 0.10 % alcoholic solution of methyl red and titrate with approximately 0.1 mol HCl until the indicator turns pink. The end point occurs before complete coagulation takes place and the color change of the indicator can be detected against the white background of the slightly coagulated latex.

11.6 *Calculation*—Calculate the total alkalinity, reported as NH₃ based on grams of NH₃ per 100 g of latex as follows:

$$\text{Total alkalinity, (as NH}_3\text{) \%} = (1.7 \times M \times n)/W \quad (3)$$

where:

M = mole of the standard HCl,