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Dual-wideband band pass filter using folded cross-stub stepped impedance resonator

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Keywords:	dual-wideband band pass filter, stepped impedance resonator, transmission zero		

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Dual-wideband band pass filter using folded cross-stub stepped impedance resonator

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Abstract:

In this letter, a dual-wideband band pass filter (DW-BPF) using cross-stub stepped impedance resonator (CS-SIR) was simulated, fabricated, and measured accordingly. The CS-SIR was used to replace the conventional half-wavelength open stub resonators. Compare to the conventional resonator, the CS-SIR resonator has a wider fractional bandwidth and ease of fabrication. Furthermore, the DB-BPF was fabricated on microstrip with $\epsilon r= 4.4$, h=0.8 mm, and tan δ = 0.0265. The DW-BPF with CS-SIR achieves transmissioncoefficients/fractional-bandwidth of 0.22 dB/94.19 % and 1.87 dB/33.52% at 1.14 GHz and 2.31 GHz, respectively. In order to reduce the filter size, a folded CS-SIR (FCS-SIR) was also proposed. As a result, this BPF size was reduced to 53%, with the BPF size of 0.30 λ_{G}^{2} and 0.14 λ_{G}^{2} for DW-BPF with CS-SIR and DW-BPF with folded CS-SIR, respectively. The λ_{G} is the wavelength at the first frequency. Further, the DW-BPF with FCS-SIR achieves transmission coefficients/fractional bandwidth of 0.19 dB/89.08 % and 1.29 dB/31.90% at 1.21 GHz and 2.41 GHz, respectively. Measured results are in a very good agreement with the simulated results.

Keywords: dual-wideband band pass filter, stepped impedance resonator, transmission zero.

1. INTRODUCTION

A dual-band band pass filter (DB-BPF) is an important component of a radio transceiver for reducing interference and noise at two frequency bands simultaneously [1]. Therefore, the pursuit of a DB-BPF with good-performances has become a key trend in the field of research. A variety of design techniques is frequently used for DB-BPF design such as square loop dual mode resonator [2], defected ground structure (DGS) [3][4], spiral resonators [5], defected stepped impedance resonator (Defected-SIR) [6][7], slotted stepped

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impedance resonator (Slotted-SIR) [8], multilayer stepped impedance resonator (Multilayer-SIR) [9][10], meandering stepped impedance resonators (Meandering-SIR) [11], stub-loaded stepped impedance resonator (Stub-loaded SIR) [12], and coupled stepped impedance resonator (Coupled-SIR) [13]. However, the DB-BPFs proposed by [1-13] still possess a complex geometry and achieve a narrow bandwidth.

As a novelty in this letter, we propose a dual-wideband band pass filter (DW-BPF) using cross-stub stepped impedance resonator (CS-SIR). Figure 1 shows a CS-SIR which was used to replace the conventional half-wavelength open stub resonators. A folded CS-SIR (FCS-SIR) was also proposed to reduce the filter size. Thus, the BPF size is reduced to 53%. The proposed design could be validated by simulations and measurements. This letter is organized as follows: section 2 briefly describes the design of the proposed DW-BPF using CS-SIR, section 3 presents the simulated and experimental results, and finally, section 4 concludes this research.

2. PROPOSED DUAL-WIDEBAND BANDPASS FILTER

A half-wavelength open stub resonator structure was commonly used to design the conventional single-band microstrip BPF [1]. In this letter, the half-wavelength open stub resonator is converted to the stub stepped impedance resonator as shown in Figure 1. The CS-SIR structure consists of three transmission lines having different characteristic impedances Z_N (N=1,2,3) with corresponding electrical lengths θ_N (N=1,2,3), respectively. Analyzing the input impedance $Z_{IN(SIR)}$ of the stepped impedance resonator section, the following equations can be derived:

$$Z_{IN(1)} = -jZ_1 \cot \theta_1 \tag{1}$$

$$Z_{IN(2)} = Z_2 \frac{Z_{IN(1)} + jZ_2 \tan \theta_2}{Z_2 + jZ_{IN(1)} \tan \theta_2}$$
(2)

$$Z_{IN(SIR)} = Z_{IN(3)} = Z_3 \frac{Z_{IN(2)} + jZ_3 \tan \theta_3}{Z_3 + jZ_{IN(2)} \tan \theta_3}$$
(3)

Equation (3) can also be expressed as:

$$Z_{IN(SIR)} = Z_1 \frac{Z_2(-jZ_3 \cot \theta_3 + jZ_2 \tan \theta_2) + jZ_1 \tan \theta_1 (Z_2 + Z_3 \cot \theta_3 \tan \theta_2)}{Z_1 Z_2 + Z_1 Z_3 \cot \theta_3 \tan \theta_2 + Z_2 Z_3 \cot \theta_3 \tan \theta_1 - Z_2^{\ 2} \tan \theta_2 \tan \theta_1}$$
(4)

The resonant frequencies can be extracted from admittance condition $Y_{IN(SIR)} = 0$ or impedance condition $Z_{IN(SIR)} = \infty$ [1]. This can be obtained when:

$$Z_2^2 \tan \theta_3 \tan \theta_1 \tan \theta_2 - Z_1 Z_2 \tan \theta_3 - Z_1 Z_3 \tan \theta_2 - Z_2 Z_3 \tan \theta_1 = 0$$
(5)

with the Z_N (N=1,2,3) and θ_N (N=1,2,3) stand for the characteristic impedance and electrical length, respectively. For the same electrical length $\theta_1 = \theta_2 = \theta_3 = \theta$, the resonance condition can also be shortened as follows:

$$\tan^3 \theta - K_1 \tan \theta - K_1 K_2 \tan \theta - K_2 \tan \theta = 0 \tag{6}$$

which can also be expressed as:

$$\tan\theta \ (\tan\theta + \sqrt{K_1 + K_1 K_2 + K_1})(\tan\theta - \sqrt{K_1 + K_1 K_2 + K_1}) = 0$$
(7)

where the impedance ratio $K_N(1,2)$ is defined by:

$$K_1 = \frac{Z_1}{Z_2}$$
, and (8)
 $K_2 = \frac{Z_3}{Z_2}$ (9)

respectively. Equation (4) shows that the resonator provides two resonating frequencies. Therefore, the resonator serves as a dual mode resonator to produce two resonant frequencies. The relationship of K_1 , K_2 , and θ is shown in Figure 2.

3. RESULT AND DISCUSSION

Figure 3 shows the schematic of the design DW-BPF using CS-SIR. The DW-BPF was fabricated on microstrip with ϵr = 4.4, h=0.8 mm, and tan δ = 0.0265. The DW-BPF

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consists of input/output port (I/O) line and two stub-SIR placed in a crossed manner. The DW-BPF was simulated by using Advanced Design System (ADS) software, whereby an RS-ZVA vector network analyzer (VNA) was used to test the fabricated prototype of DW-BPF. The dimensions are given as follows (all in millimeters): $L_1 = 32$, $L_2 = 35$, $L_3 = 9.0$, $L_4 = 23$, $L_5 = 21$, $W_1 = 2.5$, $W_2 = 1.5$, $W_3 = 5.0$, $W_4 = 10$, and $W_5 = 7.0$.

The dependency of the center frequency and fractional bandwidth on the impedance ratio (W_1/W_2) is given in Figure. 4a. The figure shows that by increasing the impedance ratio (W_1/W_2) , the center frequencies will be stable. However, increasing impedance ratio (W_1/W_2) would raise the fractional bandwidth. Figure 4b also shows the stability of the center frequency and fractional bandwidth on the variance of impedance ratio (W_3/W_2) . The chart shows that both center frequency and fractional bandwidth were not changed significantly. Figure 5(a) and 5(b) shows transmission coefficients (S_{21}) and reflection coefficients (S_{11}) in response to varied W_1 , W_3 , L_1 , and L_3 .

In order to reduce the filter size, a folded CS-SIR (FCS-SIR) was proposed as shown in Figure 6. The dimensions are given as follows (all in millimeters): $L_1 = 32$, $L_{2a} = 5$, $L_{2b} = 5$, $L_{2c} = 20$, $L_d = 5$, $L_3 = 9.0$, $L_4 = 23$, $L_5 = 21$, $W_1 = 2.5$, $W_{2a} = W_{2b} = W_{2c} = W_{2d} = 1.5$, $W_3 = 5.0$, $W_4 = 10$, and $W_5 = 7.0$. As a result, this BPF size was reduced to 53%. Furthermore, both DW-BPF using CS-SIR and folded CS-SIR (FCS-SIR) were accomplished with two pass bands. Figure 7 shows the surface current at filter with CS-SIR and FCS-SIR. It shows that the first center frequency will obtain maximum value of surface current at transmission line 2 (W_2 , L_2) and the second center frequency will obtain maximum value of surface current at transmission line 1 (W_1 , L_1) and transmission line 3 (W_3 , L_3).

Figure 8 (a) shows a comparison between simulated and measured of DW-BPF using CS-SIR. A DW-BPF with CS-SIR achieves transmission-coefficients/ fractional-bandwidth of 0.22 dB/94.19 % and 1.87 dB/33.52% at 1.14 GHz and 2.31 GHz, respectively. The

transmission zeros (TZ) of this filter are -28.29 dB, -21.36 dB, and -18.02 at 0.53 GHz, 1.79 GHz, and 2.86 GHz, respectively. Furthermore, figure 8 (b) shows a comparison between simulated and measured of DW-BPF using FCS-SIR. a DW-BPF with FCS-SIR achieves transmission coefficients/fractional bandwidth of 0.19 dB/89.08 % and 1.29 dB/31.90 % at 1.21 GHz and 2.41 GHz, respectively. The transmission zeros (TZ) of this filter are -27.94 dB, -21.25 dB, and -23.25 at 0.59 GHz, 1.90 GHz, and 3.04 GHz, respectively. Figure 9(a) shows a comparison of transmission coefficients (S₂₁) between DW-BPF using CS-SIR and DW-BPF using FCS-SIR. The measured group delays (GDs) of all pass bands below 5 ns are also depicted in Figure 9(b). Table 1 summarizes the comparison of the proposed dual band BPF. Finally, the measured results are in a very good agreement with the simulated results.

4. CONCLUSION

This letter proposes a dual-wideband band pass filter (DW-BPF) using cross-stub stepped impedance resonator (CS-SIR). The CS-SIR was used to replace the conventional half-wavelength open stub resonators. In order to reduce the filter size, a folded CS-SIR (FCS-SIR) also was proposed. As a result, this BPF size is reduced to 53%. Measured results are in a very good agreement with the simulated results. In comparison with the previous works, both of BPF using CS-SIR and BPF using FCS-SIR could produce wider bandwidth, good transmission coefficients, and ease of fabrication.

Acknowledgments

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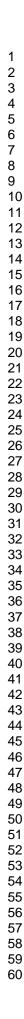
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TABLE 1.	Summary of	the proposed	dual-wideband BP	F comparison
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Ref	Method	Center Frequency (GHz)	Transmission coefficients(dB)	-3 dB FBW (%)
[2]	Square loop dual mode resonator	3.45 / 6.65	0.70 / 1.20	14.49 / 8.27
[3]	Defected ground structure (DGS)	4.60 / 7.30	0.34 / 0.35	3.87 / 2.12
[4]	Defected ground spiral resonator	1.87 / 2.43	2.00 / 2.00	4.50 / 3.30
[5]	Four spiral resonators	1.80 / 2.40	1.6 / 2.5	5.60 / 3.00
[6]	Defected stepped impedance resonator(Defected-SIR)	2.35 / 3.15	0.50 / 1.5	3.90 / 2.80
[7]	Defected stepped impedance resonator(Defected-SIR)	1.85 / 2.35	0.50 / 1.00	5.50 / 4.50
[8]	Slotted stepped impedance resonator (Slotted-SIR)	2.40 / 3.50	1.80 / 2.9	4.10 / 1.40
[9]	Multi layer stepped impedance resonator(Multilayer-SIR)	2.45 / 5.80	1.35 / 0.98	3.06 / 2.16
[10]	Multilayer stepped impedance resonator (Multilayer-SIR)	2.40 / 5.20	1.20 / 1.50	5.40 / 7.30
[11]	Meandering stepped impedance resonators (Meandering-SIR)	2.40 /5.25	0.72 / 2.10	8.33 / 3.85
[12]	Stub-loaded stepped impedance resonator (Stub-loaded SIR)	2.40 / 5.20	1.20 / 2.00	8.00 / 5.00
[13]	Coupled stepped impedance resonator (Coupled-SIR)	2.4 / 3.8	0.50 / 1.00	8.33 / 5.26
This	Cross-stub stepped impedance resonator (CS-SIR)	1.14 / 2.31	0.22 / 1.87	94.19 / 33.52
work	Folded cross-stub stepped impedance resonator (FCS-SIR)	1.21 / 2.41	0.19 / 1.29	89.08 / 31.90





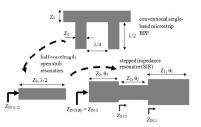


Figure 1. The conventional half-wavelength open stub resonator replaced by stub-stepped impedance resonator



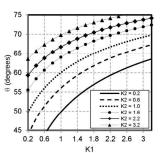
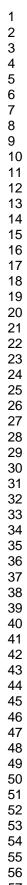
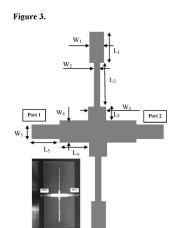


Figure 2. The relationship between impedance ratio (K1, K2) and electrical length (θ)



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The layout and photograph of the design DW-BPF using CS-SIR



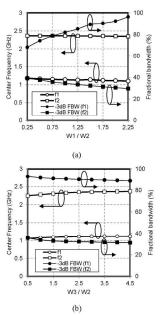
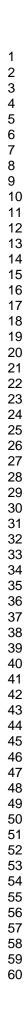


Figure 4. (a) The dependency of the center frequency and fractional bandwidth on the impedance ratio (W_1/W_2) . (b) The stability of the center frequency and fractional bandwidth on the impedance ratio (W_3/W_2) .





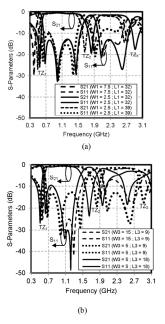


Figure 5. (a) Transmission coefficients (S_{21}) and reflection coefficients (S_{11}) response with varied W_1 and L_1 . (b) Transmission coefficients (S_{21}) and reflection coefficients (S_{11}) response with varied W_3 and L_3 .

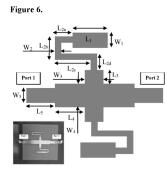
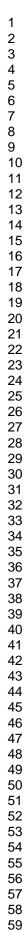


Figure 6. The layout and photograph of the design DW-BPF using Folded CS-SIR (FCS-SIR).



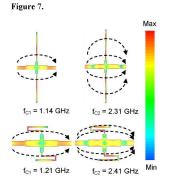


Figure 7. The surface current of the DW-BPF with CS-SIR and FCS-SIR

Figure 8.

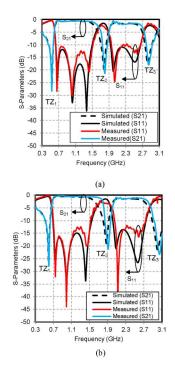
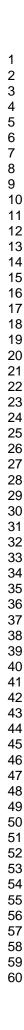


Figure 8. (a) Comparison between simulated and measured results of DW-BPF using CS-SIR. (b) Comparison between simulated and measured results of DW-BPF using FCS-SIR



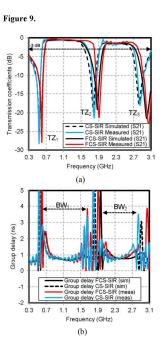


Figure 9. (a) Comparison of transmission coefficients (S₂₁) between DW-BPF using CS-SIR and DW-BPF using FCS-SIR. (b) Comparison of group delays (GDs)



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Sincerely, Teguh Firmansyah. Dept of Electrical Engineering. University of Sultan Ageng Tirtayasa. [Kutipan teks disembunyikan]

Teguh Firmansyah <teguhfirmansyah@untirta.ac.id> Kepada: supriyanto@untirta.ac.id 22 Juli 2017 pukul 15.31

Cc Pak Supriyanto

------ Forwarded message ------From: **Teguh Firmansyah** <teguhfirmansyah@untirta.ac.id> Date: 2017-07-20 11:57 GMT+07:00 Subject: Re: MOP-17-0513 - Decision To: kaichang@tamu.edu

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Article ID: MOP30848 Article DOI: 10.1002/mop.30848 Internal Article ID: 14436044 Article: Dual-wideband band pass filter using folded cross-stub stepped impedance resonator Journal: Microwave and Optical Technology Letters Corresponding email address: teguhfirmansyah@untirta.ac.id

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